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Analysis of thermal stress during of twin-roll casting of magnesium alloy

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Analysis of thermal stress during of twin-roll casting of magnesium alloy

Abstract

The process of twin-roll casting including pouring, solidifying, rolling and cooling can be accomplished in a very short time. Consequently, some important process parameters in the twin-roll casting that are difficult to be obtained in experiment can be acquired using numerical simulation. In this paper, a numerical simulation based on a 2D finite element model of vertical twin-roll strip casting of magnesium alloy has been conducted, and the thermal stress fields are significantly discussed. The influences of key process parameters consisting of submerged nozzle depth and nozzle spray angle have been studied. The thermal cracks on the surface of the strip are analysed according to the thermal stress distribution. © (2012) Trans Tech Publications, Switzerland.

Keywords

magnesium, casting, roll, alloy, twin, analysis, during, stress, thermal

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Multifactor Optimization of a Fuzzy-PID Controller using Genetic Algorithm

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Abstract - The design of a Fuzzy-PID controller involves setting the fuzzy rules, membership functions and its associated scaling factors. How to obtain a better control result and how these scaling factors affect the controller's performance are still challenge. In this paper, the automatic position control system of a Hille 100 experimental rolling mill was taken as a research object. Based on the mathematical control model of the rolling mill, a Fuzzy-PID controller was developed, and the process of implementing global optimization considering all these factors simultaneously by using genetic algorithm was introduced in detail. Through simulation, the performances of the control system with optimized multifactor Fuzzy-PID controller were given, and compared with that with only optimized fuzzy rules controller. By simulation tests, it is found that these factors will influence the control performance of the controller, and they are highly coupled with each other. The more optimized factors for a Fuzzy-PID controller, the more chance to obtain a better solution. It can also be inferred by the study that asymmetrical membership functions have more potential in improving a fuzzy controller's performance than that of symmetrical ones. The multifactor optimization method presented in this paper is verified to be feasible for developing a complex controller and can also be used to solve other complicated optimization issues.

Keywords - fuzzy-pid controller; multifactor optimization; genetic algorithm; rolling mill

I. INTRODUCTION

Hybrid fuzzy type controllers have been widely used in many industry fields, especially when the controlled objects are complex, nonlinear and time-varying. As an intelligent control strategy, Fuzzy-PID controllers have been widely used in many industrial fields due to its robustness and good adaptability when dealing with time-varying and highly nonlinear problems [1, 2]. However, the design of a Fuzzy-PID controller involves many aspects, such as the selection of membership functions and its scaling factors, fuzzy rules, inference mechanism, and the defuzzification strategy [2 - 4], etc. One of the design or tuning methods is relied on expertise knowledge, but it is limited when experts are not available, and also it cannot assure an optimum solution obtained.

So far, genetic algorithms (GA) have been adopted by many researchers to design and optimize fuzzy logic controllers. Homaifar and McCormick designed the membership functions and fuzzy rules of fuzzy controllers

simultaneously using GA [4]. In reference [5], GA was used to extract and optimize the rule base of a fuzzy PD controller and also scaling factors of the fuzzy controller were tuned with GA to improve its performance. In authors' previous work [6], the fuzzy rules of a Fuzzy-PID controller for a Hille 100 experimental rolling mill were optimized using GA. In reference [7], both a backward propagation and a genetic algorithm were adopted separately to tune the parameters of the fuzzy tension controller for a tandem rolling mill, including the scaling factors and membership functions for input and output signals, and/or rule weights. These efforts seem to be very successful.

As we know that a Fuzzy-PID controller has some self-adaptability in control process. The question is less or more factors should be optimized when designing a Fuzzy-PID controller and trying to obtain a better control performance. In addition, symmetrical membership functions were adopted for each input or output variable in most of the previous work [1-3, 5-8]. It is not clear if asymmetrical membership functions have more potential in improving the controller's performance.

In this paper, further study is carried out based on the work of reference [6]. The Fuzzy-PID roll gap control system for a Hille 100 experimental rolling mill is taken as a research object. The goal of this study is to find a method to make the control performance of the system more perfect by simultaneously optimizing the controller's fuzzy rules, asymmetrical membership functions and the ranges of the input and output variables, and as well as their influence on the control performance. Implementation of the optimization process using GA is introduced in detail. By simulation, the dynamic performance of the control system, as well as the optimized Fuzzy-PID controller are obtained and compared with the result only optimizing the fuzzy rules. Then the influence of these factors on the control performance is investigated by simulation tests. Finally, some conclusions from this study are given.

II. REVIEW OF CONTROL SYSTEM FOR HILLE 100 ROLLING MILL

In Hille 100 experimental rolling mill, two single rod cylinders, which are each controlled by a servo valve, are installed on the driving and operating sides of the mill to adjust the roll gaps. The block diagram of the position control system with a Fuzzy-PID controller can be shown in Fig. 1. K_f is the voltage conversion factor of a displacement

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transducer, U_r is the given voltage signal. The plant model is derived in reference [6], and can be expressed as Eq. (1).

$$G(s) = \frac{0.005701}{1.741e^{-14}s^5 + 1.328e^{-11}s^4 + 1.685e^{-7}s^3 + 1.128e^{-4}s^2 + 0.0775s + 1} \quad (1)$$

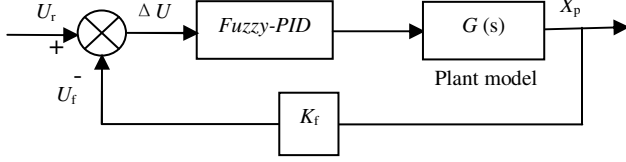


Fig. 1. Block diagram of the AGC system

III. IMPLEMENTATION OF MULTIFACTOR OPTIMIZATION OF THE FUZZY-PID CONTROLLER

Genetic algorithm is an effective and parallel method for searching global optimum solution. It is used in this study to optimize the Fuzzy-PID controller while simultaneously considering the fuzzy rules, membership functions and the ranges of the input and output variables. The process of implementing the multifactor optimization is described in the following.

A. Design of the Fuzzy-PID Controller

The designed Fuzzy-PID controller has two input and three output variables, which are error e , change in error ec , proportional gain kp , integral gain ki and derivative gain kd . The output gains can usually be expressed as Eq. (2) [1].

$$\begin{cases} kp = kp_0 + \Delta kp \\ ki = ki_0 + \Delta ki \\ kd = kd_0 + \Delta kd \end{cases} \quad (2)$$

where kp_0 , ki_0 and kd_0 are the initial values of these gains, which are set to 1.1, 20 and 0.0007, respectively. Δkp , Δki and Δkd are the change of the gains based on their initial values, they will be variables in their corresponding ranges and can be determined according to the input error e and change in error ec through fuzzy inference.

Herein, $e \in [-e_{range}, e_{range}]$, $ec \in [-ec_{range}, ec_{range}]$, $\Delta kp \in [-kp_{range}, kp_{range}]$, $\Delta ki \in [-ki_{range}, ki_{range}]$ and $\Delta kd \in [-kd_{range}, kd_{range}]$. To optimize the ranges of the input and output variables, the values of e_{range} , ec_{range} and kp_{range} , ki_{range} , kd_{range} are expressed as Eqs. (3) and (4), respectively.

$$\begin{cases} e_{range} = n_1 e_{range0} \\ ec_{range} = n_2 ec_{range0} \end{cases} \quad (3)$$

$$\begin{cases} kp_{range} = n_3 kp_{range0} \\ ki_{range} = n_4 ki_{range0} \\ kd_{range} = n_5 kd_{range0} \end{cases} \quad (4)$$

where $e_{range0}=1.0$, $ec_{range0}=120$, $kp_{range0}=1.0$, $ki_{range0}=10$, $kd_{range0}=0.0009$. $n_1 - n_5$ are scaling factors, and they are defined as $n_1 - n_5 \in [0.1, 2.1]$.

In the Fuzzy-PID controller, each of the input and output variables is assumed to have seven linguistic variables

defined as negative big (NB), negative middle (NM), negative small (NS), zero (Z), positive small (PS), positive middle (PM), positive big (PB). Apart from linguistic variable Z which has isosceles triangular-shaped membership function, all others are asymmetric triangular-shaped. Constructing a triangular-shaped membership function needs three points of values for each linguistic variable. Taking the input error e as an example, its linguistic variables in this study are defined as

$$\begin{aligned} e_{NB} &= [-e_{range}, -e_{range}, e_{NBR}], \\ e_{NM} &= [e_{NML}, -2/3e_{range}, e_{NMR}], \\ e_{NS} &= [e_{NSL}, -1/3e_{range}, e_{NSR}], \\ e_Z &= [-e_Z, 0, e_Z], \\ e_{PS} &= [e_{PSL}, 1/3e_{range}, e_{PSR}], \\ e_{PM} &= [e_{PML}, 2/3e_{range}, e_{PMR}], \text{ and} \\ e_{PB} &= [e_{PBL}, e_{range}, e_{range}]. \end{aligned}$$

where we assume that $e_{NBR} \in (-e_{range}, -1/3e_{range}]$, $e_{NML} \in [-e_{range}, -2/3e_{range})$, $e_{NMR} \in (-2/3e_{range}, 0]$, $e_{NSL} \in [-e_{range}, -1/3e_{range})$, $e_{NSR} \in (-1/3e_{range}, 1/3e_{range}]$, $e_Z \in (0, 1/3e_{range}]$, $e_{PSL} \in [-1/3e_{range}, 1/3e_{range})$, $e_{PSR} \in (1/3e_{range}, e_{range}]$, $e_{PML} \in [0, 2/3e_{range})$, $e_{PMR} \in (2/3e_{range}, e_{range}]$, and $e_{PBL} \in [1/3e_{range}, e_{range})$.

The linguistic variables of the other input and output variables are defined as the same method. Thus, there are total 55 parameters which need to be optimized for all the membership functions, and each of them is determined by its ranges defined above and its scaling factor $k(i)$ in Eq. (5).

$$k(i) = \frac{K}{2^3 - 1} \quad (5)$$

where $i=1, 2, \dots, 55$. $K \in (0, 7)$.

The fuzzy rules of the controller consist of a set of IF-THEN rules as the form

If (e is {NB... PB}) and (ec is {NB... PB}),

Then (k_p is {NB... PB}), (k_i is {NB... PB}), (k_d is {NB... PB}).

Therefore, the controller will have 49 rules, each of them contains 3 output linguistic variables corresponding to kp , ki and kd .

B. Encoding Method and Initianization

Because the operated objects are chromosomes in a genetic algorithm, all the optimized parameters should be encoded in a chromosome. In this study, binary encoding method is used for its simplicity.

According to the above design, the fuzzy rules and the membership functions have 147(=49×3) and 55 parameters (K), respectively. Each of the parameters will be encoded by a three bit binary number. The scaling factors related to the ranges of the input and output variables can be obtained by Eq. (6) in which n_i will be encoded by a six bit binary string. Thus, a chromosome with 636 (49×3×3) bits represents a possible solution.

$$\begin{cases} n_i = \frac{2n}{2^i - 1} + 0.1 \\ i = 1, 2, 3, 4, 5 \end{cases} \quad (6)$$

The initial population is set to have 50 chromosomes which are all randomly generated. The maximum generation number is set to 100. When the iteration number reaches this value, the program will automatically stop. Then the optimum solution can be obtained.

C. Other Settings

Other important settings in a genetic algorithm include the fitness function, crossover probability (P_c) and mutation probability (P_m). As in reference [6], the inverse value of the integral time absolute error (ITAE) of the system response is used as the fitness function for each chromosome. The ITAE criteria can be obtained by Eq. (7).

$$ITAE = t_s \sum_{k=1}^n (|e(k)| k t_s) \quad (7)$$

$$\alpha = \begin{cases} 100 & (e(k) < 0) \\ 1 & (e(k) \geq 0) \end{cases}$$

where t_s is the sample time, $e(k)$ is the output error in the k^{th} instance.

The crossover probability (P_c) and mutation probability (P_m) are also defined in reference [6], which are shown in Eqs. (8) and (9), respectively.

$$P_c = \begin{cases} P_{c1} - \frac{f_{avg} - f}{f_{avg}} (P_{c1} - P_{c2}) & (f < f_{avg}) \\ P_{c1} & (f \geq f_{avg}) \end{cases} \quad (8)$$

$$P_m = \begin{cases} P_{m1} & (f < f_{avg}) \\ \frac{f_{max} - f}{f_{max} - f_{avg}} P_{m1} & (f \geq f_{avg}) \end{cases} \quad (9)$$

where P_{c1} and P_{c2} are the highest and lowest crossover probability, respectively, $P_{c1}=0.8$, $P_{c2}=0.5$. P_m is the highest mutation probability, $P_{m1}=0.3$. f_{max} and f_{avg} denote the maximum and the average fitness of a population, respectively. f is the fitness of a chromosome in a population.

IV. OPTIMIZATION RESULTS

The control system for the Hille 100 experimental rolling mill shown in Fig. 1 is taken as a research object. The optimization results can be obtained by simulation and are marked with 'MOP_Fuzzy-PID'. For comparison, optimization only aiming at the fuzzy rules of the controller is also carried out and its corresponding results are marked with 'SOP_Fuzzy-PID'. In later case, the scaling factors n_1 to n_5 are set to 1.0, and the membership functions of all the input and output variables are assumed to be isosceles triangular shape with uniform distribution.

The optimized fuzzy rules for SOP_Fuzzy-PID and MOP_Fuzzy-PID are shown in Tables I and II, respectively. The scaling factors of the input and output variables for the two controllers are listed in Table III. The membership functions of e , ec , kp , ki and kd in MOP_Fuzzy-PID controller are shown in Fig. 2. From the above results, it can be found that either the fuzzy rules or the variables' scaling factors or the membership functions have changed greatly, they seem to vary irregularly. The coupling relationship among these factors has some uncertainty, therefore manually tuning these factors and finding an optimum solution may become an impossible task.

TABLE I. FUZZY RULES FOR SOP_Fuzzy-PID

K_p, k_i, k_d		Error						
		NB	NM	NS	Z	PS	PM	PB
Change in Error	NB	NM, NB, NB	PM, PS, NB	Z, PS, NM	NB, Z, NB	NM, NB, Z	PS, NB, NS	NM, NB, NB
	NM	PS, Z, NB	NB, PS, NB	PS, PS, PS	NM, NS, PM	NM, PB, NM	NS, PB, Z	NB, PM, NB
	NS	Z, NS, NB	PM, NB, NB	PM, NS, NB	PM, NM, PB	NM, NM, PB	NB, PB, PS	NM, PB, PS
	ZO	PS, NB, NB	Z, PB, PS	NM, NM, PM	NM, NB, NS	PB, NB, PB	NB, PS, NM	PB, Z, PS
	PS	NB, PS, Z	NB, PB, NM	NM, PS, Z	PM, NM, NB	PB, Z, PS	NM, Z, NB	NB, NB, PS
	PM	NB, PS, Z	NS, PM, NB	NM, NM, PS	PS, NS, PB	NS, PB, NB	NB, PM, PB	Z, NB, NB
	PB	NS, NM, PS	NM, NB, NB	NS, NS, NB	PB, NM, Z	NM, NM, PB	NB, NM, PS	PM, NB, NB

TABLE II. FUZZY RULES FOR MOP_Fuzzy-PID

K_p, k_i, k_d		Error						
		NB	NM	NS	Z	PS	PM	PB
Change in Error	NB	NB, PB, PS	NB, PB, PS	PS, NB, PM	NS, NB, PB	NB, NS, NB	PM, NB, NB	PS, NB, NS
	NM	NB, NB, Z	NB, PB, NS	NM, PB, NS	PB, NB, NM	NS, NB, PB	NS, PM, NS	NB, Z, NS
	NS	PS, PB, NM	Z, Z, Z	PS, Z, NS	NB, NS, PB	PM, NS, Z	NS, Z, NS	NS, NM, Z
	ZO	PS, NB, NB	Z, NM, NB	PS, NB, PM	NM, Z, PM	PB, PM, PM	PB, PB, PS	PM, NS, PM
	PS	NM, PS, Z	Z, PB, PM	PS, NB, NS	Z, NM, Z	PM, PS, PS	NM, PM, PS	NB, NB, PM
	PM	NM, PS, PB	NM, Z, Z	NB, NB, NB	PM, PM, NM	NM, PM, PM	NM, NB, PM	NB, NB, Z
	PB	PB, PS, PB	NB, NB, NB	NB, NB, Z	Z, NS, Z	Z, NS, NB	NS, PS, PS	PB, NB, NS

TABLE III. SCALING FACTORS OF THE INPUT AND OUTPUT VARIABLES FOR THE TWO OPTIMIZED CONTROLLERS

	n_1	n_2	n_3	n_4	n_5
SOP_Fuzzy-PID	1.00	1.00	1.00	1.00	1.00
MOP_Fuzzy-PID	1.50	0.64	1.81	1.47	1.56
MOP_Fuzzy-PID_SYMM	1.56	0.67	0.73	1.72	1.47

The step responses of the control system with the two optimized controllers are shown in Fig. 3 and their main dynamic performances are listed in Table IV. From Table IV and Fig. 3, it can be seen that after multifactor optimization, the settling time is reduced from 0.015 to 0.008 s, overshoot reduced from 4.95 to -0.056%, and ITAE is reduced from 5.94×10^{-4} to 8.0×10^{-5} , compared with that of the single-factor optimization. Thus the performance of the control system is significantly improved.

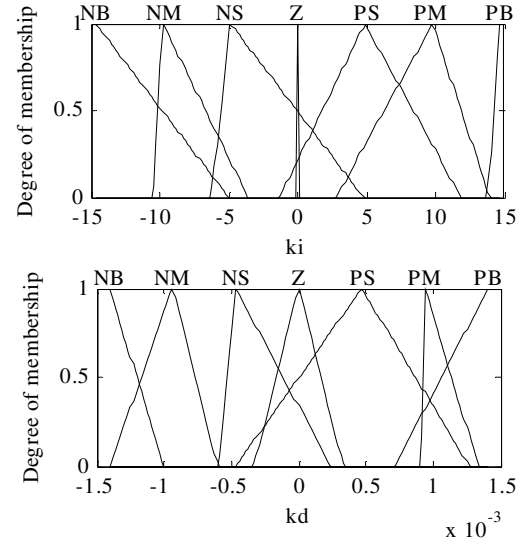
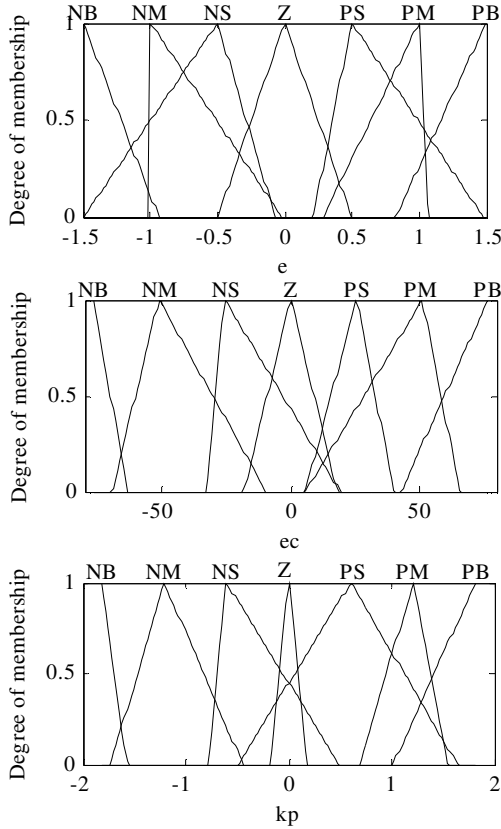


Fig. 2 Membership functions of e , ec , kp , ki , kd in MOP_Fuzzy-PID controller

TABLE IV. DYNAMIC PERFORMANCES WITH THE TWO OPTIMIZED CONTROLLERS

	Rise time (s)	Settling time (s)	Overshoot (%)	ITAE
SOP_Fuzzy-PID	0.006	0.015	4.95%	5.97×10^{-4}
MOP_Fuzzy-PID	0.006	0.008	-0.056%	8.00×10^{-5}
MOP_Fuzzy-PID_SYMM	0.007	0.014	0.3%	2.19×10^{-4}

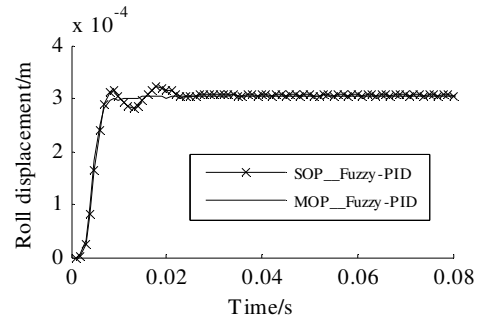


Fig. 3 Step response of the control system with two optimized controllers

V. INFLUENCE OF SOME FACTORS ON CONTROL PERFORMANCE

To understand the influence of the above optimized factors on the control performance, some simulation tests were conducted for roll gap setting of the Hille 100 experimental rolling mill.

1) Changing the scaling factors of the input and output variables ($n_1 - n_5$) separately. The results show that the dynamic performance will turn to be worse even each scaling factor is slightly changed.

2) Keeping the optimized scaling factors and fuzzy rules invariable, at the same time all the membership functions are set to be symmetrical triangular shape with uniform distribution, the step response of the control system will change badly, as shown in Fig. 4, in which it is marked with 'MOP_Fuzzy-PID_Modified'.

The above tests illustrate that the many factors in the optimized fuzzy controller are tightly coupled. For this reason, we cannot confirm that a fuzzy controller with asymmetrical membership functions is superior to that with symmetrical ones. Therefore, it is necessary to redesign the fuzzy controller with symmetrical but non-uniformly distributed triangular membership functions and re-optimize the controller from the beginning by the same method. In this case, the optimized results are marked with 'MOP_Fuzzy-PID_SYMM'. The corresponding scaling factors and dynamic performances are attached to Tables III and IV, respectively for comparison. Its step response is shown in Fig. 5.

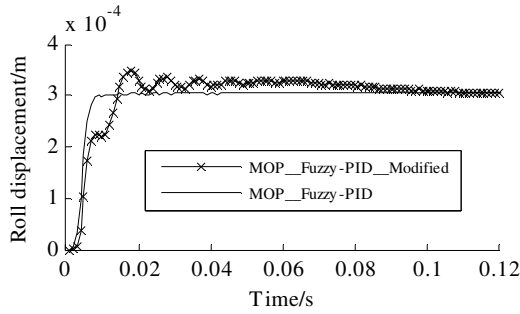


Fig. 4 Step responses of the control system with the optimum controller and its rules modified controller

It is worth noting that in order to avoid occasional results, all the optimization processes in this study were repeated 15 times and recorded. The best one for each situation is taken as the final result.

From Table III, it can be seen that only the scaling factor n_3 changed a lot and the other changed very little compared with that of 'MOP_Fuzzy-PID'. Table IV and Fig. 5 show that the dynamic performance of the system with MOP_Fuzzy-PID_SYMM controller is better than that with SOP_Fuzzy-PID controller in which only the fuzzy rules are optimized, and is worse than that with MOP_Fuzzy-PID controller in which asymmetrical membership functions are used. The phenomena give us an inspiration that the more the optimized factors for a Fuzzy-PID controller, the more chance to obtain a better solution. It can also be derived from the test results that a fuzzy type of controller with asymmetrical membership functions has better flexibility and adaptability than that with symmetrical ones. Therefore, they will help to improve the controller's performance.

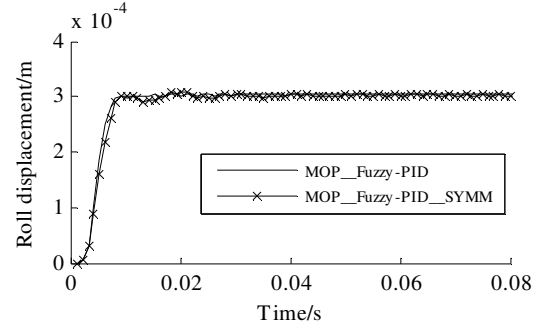


Fig. 5 Step responses of the fuzzy control system with symmetrical and asymmetrical membership functions

VI. CONCLUSION

From this study, conclusions can be obtained as follows.

1) The fuzzy rules, the membership functions and the ranges of the input and output variables in a Fuzzy-PID controller will influence the controller's control performance. The coupling relationship between these factors is very complex and unclear. When designing a Fuzzy-PID controller, the more the optimized factors, the more chance to find a better solution.

2) Compared with symmetrical membership functions, symmetrical ones have more potential in improving a fuzzy system's control performance.

3) The multifactor optimization method aiming at a Fuzzy-PID controller presented in this study is feasible and can significantly improve the controller's performance. It can also provide an effective solution for the other complex and multifactor optimization issues.

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