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2014

# Magnetization curves of sintered heavy tungsten alloys for applications in MRI-guided radiotherapy

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## Publication Details

Kolling, S., Oborn, B. M., Keall, P. J. & Horvat, J. (2014). Magnetization curves of sintered heavy tungsten alloys for applications in MRI-guided radiotherapy. *Medical Physics*, 41 (6), 061707-1-061707-6.

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# Magnetization curves of sintered heavy tungsten alloys for applications in MRI-guided radiotherapy

## Abstract

**Purpose:** Due to the current interest in MRI-guided radiotherapy, the magnetic properties of the materials commonly used in radiotherapy are becoming increasingly important. In this paper, measurement results for the magnetization (BH) curves of a range of sintered heavy tungsten alloys used in radiation shielding and collimation are presented.

**Methods:** Sintered heavy tungsten alloys typically contain > 90% tungsten and < 10% of a combination of iron, nickel, and copper binders. Samples of eight different grades of sintered heavy tungsten alloys with varying binder content were investigated. Using a superconducting quantum interference detector magnetometer, the induced magnetic moment  $m$  was measured for each sample as a function of applied external field  $H_0$  and the BH curve derived.

**Results:** The iron content of the alloys was found to play a dominant role, directly influencing the magnetization  $M$  and thus the nonlinearity of the BH curve. Generally, the saturation magnetization increased with increasing iron content of the alloy. Furthermore, no measurable magnetization was found for all alloys without iron content, despite containing up to 6% of nickel. For two samples from different manufacturers but with identical quoted nominal elemental composition (95% W, 3.5% Ni, 1.5% Fe), a relative difference in the magnetization of 11%–16% was measured.

**Conclusions:** The measured curves show that the magnetic properties of sintered heavy tungsten alloys strongly depend on the iron content, whereas the addition of nickel in the absence of iron led to no measurable effect. Since a difference in the BH curves for two samples with identical quoted nominal composition from different manufacturers was observed, measuring of the BH curve for each individual batch of heavy tungsten alloys is advisable whenever accurate knowledge of the magnetic properties is crucial. The obtained BH curves can be used in FEM simulations to predict the magnetic impact of sintered heavy tungsten alloys.

## Keywords

magnetization, sintered, mri, curves, guided, heavy, applications, alloys, tungsten, radiotherapy

## Disciplines

Engineering | Science and Technology Studies

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# Magnetization curves of sintered heavy tungsten alloys for applications in MRI-guided radiotherapy

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## Abstract

**Purpose:** Due to the current interest in MRI-guided radiotherapy, the magnetic properties of the materials commonly used in radiotherapy are becoming increasingly important. In this note, measurement results for the magnetization (BH) curves of a range of sintered heavy tungsten alloys used in radiation shielding and collimation are presented.

**Methods:** Sintered heavy tungsten alloys typically contain  $> 90\%$  tungsten and  $< 10\%$  of a combination of iron, nickel and copper binders. Samples of 8 different grades of sintered heavy tungsten alloys with varying binder content were investigated. Using a Superconducting Quantum Interference Detector (SQUID) magnetometer, the induced magnetic moment  $m$  was measured for each sample as a function of applied external field  $H_0$  and the BH curve derived.

**Results:** The iron content of the alloys was found to play a dominant role, directly influencing the magnetization  $M$  and thus the nonlinearity of the BH curve. Generally, the saturation magnetization increased with increasing iron content of the alloy. Furthermore, no measurable magnetization was found for all alloys without iron content, despite containing up to 6% of nickel. For two samples from different manufacturers but with identical quoted nominal elemental composition (95% W, 3.5% Ni, 1.5% Fe), a relative difference in the magnetization of 9 – 15% was measured.

**Conclusions:** The measured curves show that the magnetic properties of sintered heavy tungsten alloys strongly depend on the iron content, whereas the addition of nickel in the absence of iron led to no measurable effect. Since a difference in the BH curves for two samples with identical quoted nominal composition from different manufacturers was observed, measuring of the BH curve for each individual batch of heavy tungsten alloys is advisable whenever accurate knowledge of the magnetic properties is crucial. The obtained BH curves can be used in FEM simulations to predict the magnetic impact of sintered heavy tungsten alloys.

Key words: magnetization curve, sintered heavy tungsten alloy, radiation shielding, magnetic fields

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## I. INTRODUCTION

45 In recent years, the development of new modalities utilising the strengths of MRI devices for the benefit of better radiotherapy treatment has gained substantial interest. Active research in the field of MRI-guided radiotherapy is currently underway, with the first prototypes already constructed[1–3]. In this process, one major challenge to overcome is the magnetic interference between the MRI device and the hardware components of the radio-  
50 therapy treatment system which, historically, were not designed to be operated in a magnetic field. Hence, a characterisation of the magnetic properties of the materials used is essential, i.e. their magnetization or BH curves need to be known in order to predict the magnetic impact. While this information can be readily found in the literature for standard ferromagnetic materials, such as iron, nickel and common alloys of these, there is no publicly available  
55 data for the BH curves of so-called sintered heavy tungsten alloys. These alloys typically contain  $> 90\%$  tungsten (by weight); the remaining  $< 10\%$  are made up by copper, iron and nickel which serve as a binder matrix to increase ductility and machinability[4]. Due to their unique combination of high density, mechanical strength, good machinability and non-toxicity[5], they are widely used for radiation shielding and collimation purposes (e.g.  
60 in MLC's). In this note, the magnetization curves of eight grades of commercially available sintered heavy tungsten alloys have been determined experimentally with a SQUID magnetometer.

## II. METHODS AND MATERIALS

### A. Sintered heavy tungsten alloy samples

65 Table I lists the eight samples of sintered heavy tungsten alloys the magnetization curves of which were experimentally determined. The samples were provided by the two distributors Midwest Tungsten Service[6] and Wolfmet[7]. The selected grades differed in elemental composition, with an iron content varying from  $3\%$  down to  $0\%$ . The three iron-free samples contained between  $6\%$  and  $3.5\%$  of the relatively less-ferromagnetic nickel. The  $F_x N_x$   
70 sample was cut from a decommissioned Varian Millennium 120 MLC leaf. Although the exact elemental composition was unknown, obtaining the BH curve of this sample was of particular interest due to its widespread use in MLC's. The two samples referred to as

TABLE I. List of sintered heavy tungsten alloy samples examined in this study. Grades marked with <sup>1</sup> or <sup>2</sup> were provided by Midwest Tungsten Service[6] or Wolfmet[7], respectively.

Sample	Elem. composition (wt%)				Grade
	W	Fe	Ni	Cu	
$F_xN_x$	—	—	—	—	MLC
$F_{3.0}N_{7.0}$	90.0	3.0	7.0	0.0	MT17F <sup>1</sup>
$F_{1.5}N_{3.5}$	95.0	1.5	3.5	0.0	MT18F <sup>1</sup>
$F_{1.5}N'_{3.5}$	95.0	1.5	3.5	0.0	HE395 <sup>2</sup>
$F_{0.9}N_{2.1}$	97.0	0.9	2.1	0.0	MT185 <sup>1</sup>
$F_{0.0}N_{6.0}$	90.0	0.0	6.0	4.0	MT17C <sup>1</sup>
$F_{0.0}N_{4.0}$	95.0	0.0	4.0	1.0	HA195 <sup>2</sup>
$F_{0.0}N_{3.5}$	95.0	0.0	3.5	1.5	MT18C <sup>1</sup>

$F_{1.5}N_{3.5}$  and  $F_{1.5}N'_{3.5}$  were quoted with identical nominal composition, but were produced by different manufacturers. Comparing the results for these samples will indicate if knowledge  
75 of the nominal elemental composition (as quoted by the manufacturer) is sufficient to predict the magnetization curve of a sample with respect to a measured reference curve with the same quoted nominal composition. In preparation for the experiments, the samples were cut into cubic blocks of  $3 \times 3 \times 3 \text{ mm}^3$  to fit into the loader cup of the measurement device.

## B. Measurement of magnetic moment

80 A SQUID magnetometer (Magnetic Property Measurement System 5XL, Quantum Design) was used to determine the magnetic moment  $m$  of the sintered heavy tungsten alloy samples. The measurements were carried out at a temperature of 300 K. Starting from a fully demagnetized sample, the magnetometer measured the magnetic moment  $m$  induced in the sample of the sintered heavy tungsten alloy as a function of applied external field  $H_0$  in  
85 the range of 0 to  $8 \times 10^5 \text{ A/m}$ . Data points were acquired with a step width of  $6 \times 10^3 \text{ A/m}$  in the low-field range from 0 to  $90 \times 10^3 \text{ A/m}$ ; the step width was increased to  $40 \times 10^3 \text{ A/m}$  and  $80 \times 10^3 \text{ A/m}$  above  $90 \times 10^3 \text{ A/m}$  and  $240 \times 10^3 \text{ A/m}$ , respectively. The magnetization curve of the MLC-leaf sample had already been determined in a related research project where

the step widths in the measurement sequence were slightly different[8]. Since sampling the  
90 magnetization curves with the exact same point density was not necessary for this work, the  
previously obtained data was used (see Table II in the supplemental data).

### C. Data analysis

The magnetic moment  $m$  was normalized by the sample volume, yielding the volume-  
independent magnetization  $M$ . In materials of finite length, magnetic poles are generated  
95 near the ends of the sample which gives rise to a demagnetizing field  $H_d$  opposing the applied  
field  $H_0$ [9]:

$$H_d = N_d M, \quad (1)$$

where the constant of proportionality  $N_d$  is called demagnetizing factor. For the demag-  
netizing factor, the approximate expression  $N_d = 1/(2n + 1)$  for a uniformly magnetized  
100 rectangular rod was used[10]. The dimensional ratio  $n$  was 1 for our cubic samples. Sub-  
traction of the demagnetizing field  $H_d$  from the applied field  $H_0$  yields the internal field

$$H = H_0 - H_d. \quad (2)$$

Then, the magnetic flux density  $B$  was derived according to the fundamental relation

$$B(H) = \mu_0(H + M), \quad (3)$$

105 where  $\mu_0$  is the vacuum permeability[9].

### D. Error analysis

The SQUID magnetometer provides the values for the applied magnetic field with a  
relative accuracy of  $\frac{\sigma_H}{H} = 10^{-7}$ . Furthermore, the relative sensitivity for the measurement of  
the magnetic moment is quoted by the manufacturer as  $\frac{\sigma_m}{m} = 10^{-4}$ [11]. The samples were cut  
110 into cubic blocks with 3.00 mm edge length by the University of Wollongong workshop with  
an accuracy of  $\pm 0.05$  mm. In order to reduce the measurement uncertainty, the dimensions  
of each tungsten sample have been measured with calipers to an uncertainty in the edge

lengths  $l$  of  $\sigma_l = 0.01$  mm. Hence, the uncertainties in the magnetisation  $M$  and magnetic flux density  $B$  could be derived as

$$\sigma_M = \sqrt{\left(\frac{\partial M}{\partial l}\sigma_l\right)^2 + \left(\frac{\partial M}{\partial m}\sigma_m\right)^2} \approx \frac{\partial M}{\partial l}\sigma_l = 0.01M \quad (4)$$

and

$$\sigma_B = \sqrt{\left(\frac{\partial B}{\partial M}\sigma_M\right)^2 + \left(\frac{\partial B}{\partial H}\sigma_H\right)^2} \approx \frac{\partial B}{\partial M}\sigma_M = 0.01\mu_0M, \quad (5)$$

where the two neglected terms associated with  $\sigma_m$  and  $\sigma_H$  were more than  $10^2$  times smaller compared to the dominant terms associated with  $\sigma_l$  and  $\sigma_M$ , respectively. Essentially, the accuracy of the experimental data is limited by the uncertainty in the edge lengths.

### III. RESULTS AND DISCUSSION

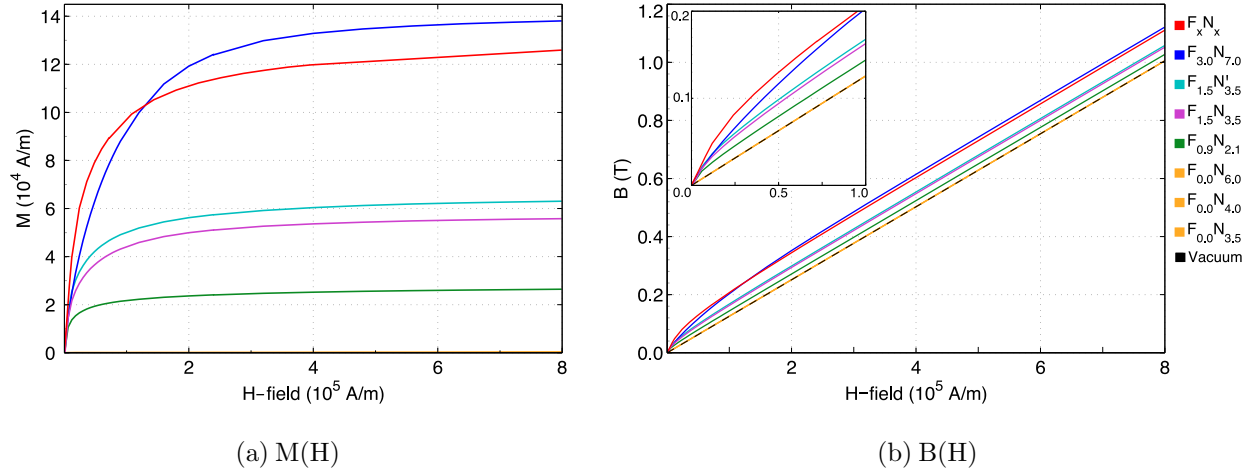


FIG. 1. Measured  $M(H)$  and  $B(H)$  curves of eight different sintered heavy tungsten alloys. The saturation magnetization increases with the iron content of the alloys. Despite up to 6% nickel content, the samples without iron show no measurable magnetization. The  $F_{1.5}N_{3.5}$  and  $F_{1.5}N'_{3.5}$  samples with identical quoted nominal composition show a relative difference in the magnetization of 11 – 16%. The uncertainties in the measurement data are too small to be visualized, but are disclosed in the Supplemental Data V.

The magnetization  $M$  measured in the H-field range of  $0 - 8 \times 10^5$  A/m is shown in Fig. 1(a) and the corresponding BH curves in Fig. 1(b). As a general trend in Fig. 1(a), the magnetization  $M(H)$  becomes higher as the iron content of the sintered heavy tungsten alloy increases. For instance, a maximum saturation magnetization of about  $14 \times 10^4$  A/m



is reached for the  $F_{3.0}N_{7.0}$  sample. The alloys with 1.5% iron, half the iron of the  $F_{3.0}N_{7.0}$  sample, saturate at around  $6 \times 10^4$  A/m; the sample with 0.9% iron at around  $2.5 \times 10^4$  A/m. The sample cut from the Varian Millennium 120 MLC leaf shows the steepest initial increase of the magnetization  $M$  with  $H$  which then flattens out and crosses the  $F_{3.0}N_{7.0}$  curve at  $M \approx 10 \times 10^4$  A/m, before levelling off at about  $13 \times 10^4$  A/m. Such a saturation magnetization, seen in the context of the curves of the other alloys, could be a sign of an iron content somewhere between 1.5% and 3% (probably closer to the latter value).

Independent of their respective nickel content, no measurable magnetization was found for any of the three alloys without iron, which is in agreement with the results for a measured W-Ni-Cu heavy tungsten alloy found in the literature[12]. These findings suggest that a nickel content of up to 6% is uncritical with regards to magnetic properties and such alloys may be used in environments with magnetic fields without concern.

The two samples with identical quoted nominal elemental composition,  $F_{1.5}N_{3.5}$  and  $F_{1.5}N'_{3.5}$ , follow a similar course, however are not in perfect agreement: A maximum relative difference in  $M$  of 16% is observed at low  $H$  which levels off at about 11% in the regime of magnetic saturation. This discrepancy relates to a maximum difference of 9% in the initial section of the corresponding  $BH$  curves (Fig. 1(b)). Above magnetic saturation,  $B$  and  $H$  are linked through a linear relation with a slope of  $\mu_0$  (Eq. 3) and hence the absolute difference between the curves remains constant. The difference can be expressed through the difference in the saturation magnetizations of both samples and amounts to  $\Delta B_{sat} = \mu_0 \Delta M_{sat} \approx 6$  mT. Considering an uncertainty in the magnetisation of  $\sigma_M = 1\%M$  (as discussed in Section II D), it can be ruled out that the observed difference in the range of  $11 - 16\%M$  is a measurement artefact.

A number of factors comes to mind that could possibly explain the difference: The actual elemental compositions of the two samples could be slightly different from what is quoted since the manufacturers work to a relatively broad tolerance and some variation in the composition between batches is likely. The different sintering procedures used by the manufacturers may have an influence on the magnetic properties by affecting the size and local concentration of the magnetic ions within the alloy. In addition, the grain structure of the constituent metal particles as well as unintentional annealing following the actual sintering may also play a part. In the literature, differences in the magnetization curves for two samples with identical elemental composition (but one in as-sintered, the other in

cold-worked condition) have been reported[13] and support this claim. No further steps were undertaken to identify how big a role each of these factors plays in the examined samples as this was not within the scope of this work. However, regardless of which is the dominant factor, the observed difference makes clear that, whenever accurate knowledge of the magnetic properties is crucial, a reference BH curve for an alloy with the same quoted nominal composition may not be sufficient to predict the magnetic impact of sintered heavy tungsten alloys from other manufacturers or even another batch of the same manufacturer. Instead, BH curves should ideally be measured for each individual batch of heavy tungsten alloys in such cases.

#### IV. CONCLUSION

Through the measurement of the magnetization curves of eight sintered heavy tungsten alloys, it could be shown that the magnetic properties of sintered heavy tungsten alloys strongly depend on the iron content of the alloys, whereas the addition of up to 6 % of nickel in the absence of iron led to no measurable effect. Furthermore, the observed difference in the BH curves for two samples with identical nominal composition but from different manufacturers indicates that the BH curve should be measured for each individual batch of heavy tungsten alloys whenever accurate knowledge is crucial. Using these BH curves as input for FEM simulations to predict the magnetic impact of sintered heavy tungsten alloys will be a great help in the development of new MR-based imaging and treatment modalities in radiotherapy.

#### V. SUPPLEMENTAL DATA

See Table II below for the measurement data.

#### ACKNOWLEDGMENTS

We thank the Midwest Tungsten Service and Wolfmet companies for the free supply of the tungsten alloy samples used in this study. Furthermore, we gratefully acknowledge funding

TABLE II. Data of the measured BH curves.

(a) $F_{3.0}N_{7.0}$		(b) $F_{1.5}N_{3.5}$		(c) $F_{1.5}N'_{3.5}$		(d) $F_{0.9}N_{2.1}$	
$H (\frac{\text{Å}}{m})$	$B \pm \sigma_B$ (mT)	$H (\frac{\text{Å}}{m})$	$B \pm \sigma_B$ (mT)	$H (\frac{\text{Å}}{m})$	$B \pm \sigma_B$ (mT)	$H (\frac{\text{Å}}{m})$	$B \pm \sigma_B$ (mT)
0	0.00 ± < 0.01	0	0.00 ± < 0.01	0	0.00 ± < 0.01	0	0.00 ± < 0.01
5811	19.22 ± 0.35	5901	19.55 ± 0.36	5910	21.44 ± 0.42	5937	16.40 ± 0.27
11909	35.78 ± 0.62	11981	33.35 ± 0.55	11990	36.57 ± 0.65	12008	26.64 ± 0.34
17900	50.33 ± 0.82	17972	44.37 ± 0.65	17972	48.01 ± 0.77	17981	35.57 ± 0.39
24007	64.17 ± 1.01	24052	54.63 ± 0.73	24070	58.58 ± 0.86	24070	44.24 ± 0.42
29989	77.02 ± 1.17	30034	64.19 ± 0.79	30043	68.32 ± 0.92	30043	52.51 ± 0.44
35961	89.35 ± 1.31	36006	73.38 ± 0.84	36024	77.69 ± 0.98	36015	60.62 ± 0.46
42015	101.41 ± 1.44	42051	82.44 ± 0.88	42060	86.86 ± 1.03	42051	68.71 ± 0.47
47987	112.96 ± 1.56	48023	91.17 ± 0.92	48032	95.70 ± 1.07	48023	76.63 ± 0.48
53942	124.18 ± 1.67	53978	99.74 ± 0.95	53978	104.34 ± 1.10	53969	84.46 ± 0.50
59968	135.25 ± 1.77	60004	108.28 ± 0.98	60013	112.98 ± 1.13	59995	92.34 ± 0.50
65896	145.91 ± 1.87	65941	116.62 ± 1.01	65932	121.32 ± 1.16	65914	100.05 ± 0.51
71904	156.49 ± 1.96	71931	124.91 ± 1.03	71931	129.70 ± 1.19	71922	107.85 ± 0.52
77877	166.83 ± 2.04	77904	133.12 ± 1.05	77913	137.95 ± 1.21	77895	115.58 ± 0.53
83885	177.04 ± 2.12	83912	141.30 ± 1.07	83921	146.18 ± 1.23	83903	123.33 ± 0.53
89993	187.19 ± 2.20	90020	149.57 ± 1.09	90020	154.47 ± 1.25	90002	131.17 ± 0.54
119963	234.98 ± 2.50	119990	189.56 ± 1.16	119990	194.53 ± 1.32	119999	169.59 ± 0.56
159810	295.03 ± 2.79	159837	241.69 ± 1.22	159837	246.72 ± 1.38	159828	220.32 ± 0.58
199801	351.51 ± 2.98	199810	293.30 ± 1.26	199819	298.44 ± 1.43	199810	271.05 ± 0.59
239711	405.82 ± 3.10	239729	344.43 ± 1.29	239738	349.64 ± 1.46	239729	321.59 ± 0.6
239720	405.67 ± 3.09	239729	344.38 ± 1.29	239747	349.60 ± 1.46	239747	321.58 ± 0.6
319620	511.05 ± 3.24	319638	446.16 ± 1.33	319656	451.54 ± 1.51	319647	422.57 ± 0.62
399566	614.07 ± 3.32	399575	547.44 ± 1.35	399593	553.00 ± 1.54	399584	523.42 ± 0.63
479448	715.97 ± 3.36	479457	648.42 ± 1.37	479475	654.12 ± 1.56	479475	624.12 ± 0.64
559313	817.40 ± 3.39	559331	749.22 ± 1.38	559349	755.02 ± 1.57	559331	724.71 ± 0.65
639313	918.69 ± 3.42	639348	850.10 ± 1.39	639367	855.98 ± 1.59	639348	825.45 ± 0.66
719330	1019.81 ± 3.43	719366	950.92 ± 1.40	719366	956.82 ± 1.60	719348	926.14 ± 0.66
799204	1120.63 ± 3.45	799240	1051.50 ± 1.41	799258	1057.49 ± 1.60	799276	1026.72 ± 0.66

(e) $F_{0.0}N_{6.0}$		(f) $F_{0.0}N_{4.0}$		(g) $F_{0.0}N_{3.5}$		(h) $F_xN_x$	
$H (\frac{\text{Å}}{m})$	$B \pm \sigma_B$ (mT)	$H (\frac{\text{Å}}{m})$	$B \pm \sigma_B$ (mT)	$H (\frac{\text{Å}}{m})$	$B \pm \sigma_B$ (mT)	$H (\frac{\text{Å}}{m})$	$B \pm \sigma_B$ (mT)
0	0 ± < 0.01	0	0.00 ± < 0.01	0	0.00 ± < 0.01	0	0.00 ± < 0.01
5901	7.42 ± < 0.01	5829	7.32 ± < 0.01	5892	7.40 ± < 0.01	3904	16.31 ± 0.34
11981	15.06 ± < 0.01	11918	14.97 ± < 0.01	11972	15.05 ± < 0.01	7978	33.25 ± 0.70
17963	22.58 ± < 0.01	17909	22.51 ± < 0.01	17954	22.57 ± < 0.01	11990	48.56 ± 1.00
24052	30.23 ± < 0.01	23998	30.16 ± < 0.01	24052	30.23 ± < 0.01	12071	48.78 ± 1.01
30034	37.74 ± < 0.01	29989	37.69 ± < 0.01	30025	37.74 ± < 0.01	24025	80.69 ± 1.51
36006	45.25 ± < 0.01	35997	45.24 ± < 0.01	35997	45.25 ± < 0.01	35979	104.85 ± 1.79
42051	52.85 ± < 0.01	42006	52.79 ± < 0.01	42051	52.86 ± < 0.01	48032	126.53 ± 1.99
48023	60.35 ± < 0.01	47978	60.29 ± < 0.01	48014	60.35 ± < 0.01	59977	146.41 ± 2.13
53978	67.84 ± < 0.01	53933	67.78 ± < 0.01	53960	67.83 ± < 0.01	71922	165.34 ± 2.25
60004	75.41 ± < 0.01	59968	75.36 ± < 0.01	59995	75.41 ± < 0.01	71976	165.25 ± 2.24
65923	82.85 ± < 0.01	65896	82.81 ± < 0.01	65923	82.87 ± < 0.01	108009	218.92 ± 2.50
71931	90.40 ± < 0.01	71895	90.35 ± < 0.01	71922	90.41 ± < 0.01	143826	268.92 ± 2.65
77913	97.91 ± < 0.01	77877	97.87 ± < 0.01	77895	97.91 ± < 0.01	179778	317.48 ± 2.75
83921	105.47 ± < 0.01	83903	105.44 ± < 0.01	83930	105.50 ± < 0.01	215830	365.27 ± 2.82
90029	113.14 ± < 0.01	89993	113.09 ± < 0.01	90011	113.14 ± < 0.01	251737	412.22 ± 2.88
120008	150.82 ± < 0.01	119972	150.77 ± < 0.01	120008	150.85 ± < 0.01	287707	458.89 ± 2.92
159855	200.89 ± < 0.01	159828	200.86 ± < 0.01	159855	200.93 ± < 0.01	323767	505.37 ± 2.96
199837	251.14 ± < 0.01	199819	251.11 ± < 0.01	199828	251.18 ± < 0.01	359710	551.60 ± 2.99
239756	301.30 ± < 0.01	239729	301.27 ± < 0.01	239747	301.36 ± < 0.01	395662	597.53 ± 3.01
239765	301.31 ± < 0.01	239738	301.27 ± < 0.01	239747	301.36 ± < 0.01	799258	1109.87 ± 3.16
319674	401.74 ± < 0.01	319638	401.68 ± < 0.01	319665	401.81 ± < 0.01		
399611	502.19 ± < 0.01	399575	502.14 ± < 0.01	399602	502.29 ± < 0.01		
479493	602.58 ± < 0.01	479466	602.54 ± < 0.01	479484	602.70 ± < 0.01		
559349	702.93 ± < 0.01	559331	702.90 ± < 0.01	559349	703.09 ± < 0.01		
639366	803.49 ± < 0.01	639348	803.46 ± < 0.01	639366	803.67 ± < 0.01		
719384	904.05 ± < 0.01	719366	904.02 ± < 0.01	719402	904.28 ± < 0.01		
799258	1004.42 ± < 0.01	799258	1004.41 ± < 0.01	799258	1004.65 ± < 0.01		

through the NHMRC Program Grant 1036078 and ARC Discovery Grant DP120100821.

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