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Abstract

An octave spanning spectrum is generated in an As₂S₃ taper via 77 pJ pulses from an ultrafast fiber laser. Using a previously developed tapering method, we construct a 1.3 μm taper that has a zero-dispersion wavelength around 1.4 μm. The low two-photon absorption of sulfide-based chalcogenide fiber allows for higher input powers than previous efforts in selenium-based chalcogenide tapered fibers. This higher power handling capability combined with input pulse chirp compensation allows an octave spanning spectrum to be generated directly from the taper using the unamplified laser output.

Keywords

pulse, pump, taper, energy, octave, ultralow, spanning, supercontinuum, as₂s₃

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Octave spanning supercontinuum in an As_2S_3 taper using ultralow pump pulse energy

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An octave spanning spectrum is generated in an As_2S_3 taper via 77 pJ pulses from an ultrafast fiber laser. Using a previously developed tapering method, we construct a $1.3\text{ }\mu\text{m}$ taper that has a zero-dispersion wavelength around $1.4\text{ }\mu\text{m}$. The low two-photon absorption of sulfide-based chalcogenide fiber allows for higher input powers than previous efforts in selenium-based chalcogenide tapered fibers. This higher power handling capability combined with input pulse chirp compensation allows an octave spanning spectrum to be generated directly from the taper using the unamplified laser output. © 2011 Optical Society of America

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The generation of supercontinuum spectra in optical fiber has played an important role in many technologies, such as optical coherence tomography [1], spectroscopy [2], and frequency metrology [3]. In particular, when an octave of bandwidth is achieved, a mode-locked laser can be used as a frequency comb generator via the f - $2f$ interferometer technique [4]. However, achieving such large bandwidths requires pulse energies on the order of nanojoules, thus imposing constraints on the requisite power level. The typical arrangement for generating an octave with an erbium-based mode-locked laser involves dispersion compensation and an optical amplifier before entering a section of highly nonlinear fiber. On top of the added complexity, the amplifier adds amplified spontaneous emission noise to the output, thereby reducing the ultimate signal-to-noise achievable in an optical frequency measurement [5].

In this Letter, we present a sulfide-based chalcogenide taper that is capable of generating over one octave of bandwidth at a pulse energy of only 77 pJ, using a standard, unamplified mode-locked erbium fiber laser. Furthermore, at higher pulse energies, the octave spanning spectrum becomes extremely flat, with an octave contained within the -10 dB points.

Apart from the potential usefulness of chalcogenide-based glasses in the mid-IR wavelength range [6] (where they are transparent), the chalcogenides also have a stronger nonlinearity than standard silica-based fibers in the telecommunications wavelength range. This high nonlinearity, combined with the strong modal confinement due to the large index contrast, yields nonlinear parameters that are typically 2 orders of magnitude larger than tapered silica fibers [7].

Previous experiments with chalcogenide planar waveguides [8,9] have demonstrated the ability to engineer dispersion by controlling the waveguide geometry. Similarly, in a fiber waveguide, tapering provides the means to not only dramatically increase the nonlinear parameter of the fiber device γ , but to also engineer the total dispersion from normal to zero or even anomalous (see Fig. 1). This fact is crucial to using chalcogenide devices

for supercontinuum generation in the telecommunications window because the material dispersion of chalcogenide at this wavelength is large and normal (-360 ps/nm km). The tapering process used in this work was previously developed [10,11] for As_2S_3 fiber. The end result is a tapered region with a mode area (A_{eff}) of just $0.8\text{ }\mu\text{m}^2$, which increases γ to $12,400\text{ W}^{-1}\text{km}^{-1}$ at 1550 nm . Thus, the nonlinearity of the tapered fiber competes well with more exotic construction techniques [12]. Silica glass fiber leads were used to butt-couple the input pulses into the chalcogenide fiber, and used to outcouple the broad spectrum from the output end of the taper. An

Fig. 1. (Color online) Taper details. (a) Nonlinearity (left vertical axis) and effective mode area (right vertical axis) as a function of fiber diameter. The nonlinear parameter mirrors the effective mode area, and reaches extremely large values only when the fiber diameter goes below $4\text{ }\mu\text{m}$. (b) Dispersion profile of the As_2S_3 fiber as a function of taper diameter. The untapered fiber exhibits large, normal dispersion. The effect of tapering is to introduce anomalous waveguide dispersion, which eventually shifts the total dispersion to zero and beyond.

FC/APC connector is used to couple the laser output into the taper device, and the final result is a robust device that has 5.7 dB pigtail-to-pigtail insertion loss (split between 2.2 dB Fresnel loss and 3.5 dB propagation loss). In principle, the lumped propagation loss can be reduced through improvements in the tapering and silica–chalcogenide butt-coupling.

The input pulses to the As_2S_3 fiber taper are generated from an erbium-fiber-based mode-locked laser (see Fig. 2). This laser is mode locked using the nonlinear polarization rotation scheme and produces 250 fs pulses at a 38.6 MHz repetition frequency with 17 mW of average power. As the untapered region of the chalcogenide fiber presents significant normal dispersion, the input pulses to the taper device must be compensated by an equivalent amount of anomalous prechirp. The As_2S_3 input fiber used in this experiment constitutes a net group-delay dispersion (GDD) of 0.114 ps^2 . Experimentally, the best dispersion compensation (as judged by bandwidth produced) for this GDD required 5 m of SMF-28 fiber, in good agreement with the calculated ratio of dispersion and length (i.e. $|\beta_{2,\text{As}_2\text{S}_3}/\beta_{2,\text{SMF-28}}| = 21.1$ and $l_{\text{SMF-28}}/l_{\text{As}_2\text{S}_3} = 20.2$). Frequency-resolved-optical-gating (FROG) measurements were performed on the chirped input pulses using a commercial FROG device. The recorded spectrograms and the corresponding time domain electric field envelopes of the direct laser output and the prechirped pulses can be seen in Fig. 3. These electric field envelopes were used as input pulses in the numerical modeling. The average power of the input pulses was tuned using an in-line variable optical attenuator.

Detection of the output spectra from the taper was accomplished using three separate spectrometers. The short wavelength side (800–1200 nm) was measured using an ANDO AQ6375, the middle wavelengths

Fig. 2. (Color online) Experimental layout. Pulses from the erbium laser are prechirped using 5 m of silica fiber ($\beta_2 = -0.021 \text{ ps}^2/\text{m}$), while the variable optical attenuator (VOA) is used to vary the average power. A FROG is used to retrieve the full electric field that is used in the simulation. Light is coupled into the chalcogenide fiber via a butt-coupled silica fiber that is affixed with UV-cured epoxy. The output of the taper device is measured individually with three spectrometers covering various wavelength ranges. While optical spectrum analyzer (OSA) 1 and OSA 2 are fiber coupled, OSA 3 is free-space coupled and allows for sensitive detection of the long wavelength edge.

Fig. 3. (Color online) Experimental spectrograms and retrieved electric fields. (a) Shortest pulse achievable from the mode-locked laser. (b) Pulse as it appears just before entering the taper device. The pulse in (b) was used in the numerical model.

(1200–1900 nm) using a Yokogawa AQ6315, and the long wavelengths ($>1900 \text{ nm}$) using a free-space scanning monochromator and a liquid-nitrogen-cooled mercury–cadmium–telluride detector. While the measurement bandwidth of the Yokogawa was large enough to cover the range of interest (out to 2400 nm), care had to be taken to avoid recording a false signal at the longer wavelengths due to the second-order diffraction from the grating. To avoid this, a 1500 nm long-pass filter was used in conjunction with the free-space spectrometer for the long wavelength regions.

The output spectra of the taper are shown in Fig. 4. As the power is incrementally increased, the spectrum

Fig. 4. (Color online) Output spectra from the As_2S_3 taper (top) and numerical simulation (bottom). As the peak power is steadily increased, the supercontinuum generation achieves one octave of bandwidth (-20 dB points) at 150 W peak power. At the highest peak power (824 W), an octave is contained within the -10 dB points, and the long wavelength edge is extending into the mid-IR regime ($>2 \mu\text{m}$). The spike at the center of the spectra is a long pulse pedestal ($>10 \text{ ps}$) on the laser output, and has a minimal contribution to the broadening.

begins to broaden to several hundred nanometers with relatively low peak powers, as has been previously reported [13]. With 77 pJ of pulse energy (150 W peak power, 3 mW average power), the -20 dB bandwidth covers the span from 970 to 1990 nm, over one octave of optical bandwidth. The short wavelength, phase-matched dispersive wave is clearly visible at peak powers above 25 W, while Raman shifting solitons are responsible for extending the bandwidth in the long wavelength side. For the highest peak power, the soliton number ($N = \sqrt{L_D/L_{NL}}$, where L_D is the dispersion length and L_{NL} is the nonlinear length) is of the order of 50, while the fission length is of the order of 5 mm. This results in a large number of spectrally broad, overlapping soliton features [14] that shed energy into resonant dispersive waves over a wider bandwidth [15], while noise-induced fission of the initial pulse induces shot-to-shot variation, resulting in a smoothing effect that produces a remarkably flat spectrum (an octave is contained within the -10 dB points). Using the measured taper parameters in conjunction with an adaptive split-step Fourier routine, we were able to accurately model the experimental results (Fig. 4, bottom) by numerically solving the nonlinear Schrödinger equation.

In conclusion, we have demonstrated an octave spanning spectrum in a sulfide-based chalcogenide tapered fiber using only 77 pJ pulse energy, to our knowledge the lowest ever reported for octave generation in a taper [7]. These results were obtained by carefully tailoring the input pulse chirp and utilizing the robust power handling capabilities of sulfide. These results could find use in applications such as f - $2f$ interferometers used in frequency combs. The taper coupling method presented here allows the experimenter to easily and efficiently couple light into the taper via standard APC connectors. In addition, the low power required for octave generation in this taper relaxes the power requirement of standard octave spanning generation [16], and could potentially remove the need for an amplifier in such a system. Future work will involve investigating the long wavelength side of the spectral generation for mid-IR applications. Through dispersion engineering in the taper, it may be possible to utilize the soliton self-frequency shift to achieve highly efficient spectral shifting to wavelengths beyond 2 μ m.

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