

2021

## Human-device interface pressure measurement in prosthetic, orthotic and exoskeleton applications: A systematic review

Lucy E. Armitage  
*University of Wollongong, [alucy@uow.edu.au](mailto:alucy@uow.edu.au)*

Shruti Turner  
*Imperial College London*

Manish Sreenivasa  
*University of Wollongong, [manishs@uow.edu.au](mailto:manishs@uow.edu.au)*

Follow this and additional works at: <https://ro.uow.edu.au/test2021>

---

### Recommended Citation

Armitage, Lucy E.; Turner, Shruti; and Sreenivasa, Manish, "Human-device interface pressure measurement in prosthetic, orthotic and exoskeleton applications: A systematic review" (2021). *Scopus Harvesting Series*. 2730.  
<https://ro.uow.edu.au/test2021/2730>

---

## Human-device interface pressure measurement in prosthetic, orthotic and exoskeleton applications: A systematic review

### Abstract

This study aimed to investigate normal and shear load sensor technology that has been characterised and used at the human-device interface in prosthetic, orthotic and exoskeleton applications. In addition to taking a cross-disciplinary view, this study expands on previous reviews by considering recently published papers, clinical translation of sensors, and development of the sensor technology itself. A search of MEDLINE, INSPEC, SCOPUS and Web of Science was performed up to 26 January 2021. A total of 33 studies were assessed for quality and their data extracted. The review found variable quality of published papers, with normal load being most commonly measured, and resistive sensor technology most commonly used. The translation to clinical environments was indicated in most studies, though the study population was not always made up of the target users. Studies could benefit from more direct comparison with clinically relevant load thresholds and by ensuring clinical testing is performed in the most realistic and representative way possible. Additionally, more focus on developing sensors that measure shear loads would enable further insights into conditions at the human-device interface. Finally, all researchers would benefit from better and more widespread anonymous data sharing practices to facilitate further experimentation.

1 **Title:** Human-device interface pressure measurement in prosthetic, orthotic and exoskeleton  
2 applications: A systematic review

3 **Authors:**

4 Lucy Armitage<sup>a</sup> – [alucy@uow.edu.au](mailto:alucy@uow.edu.au) – Corresponding author for all stages

5 Shruti Turner<sup>b</sup> - [s.turner17@imperial.ac.uk](mailto:s.turner17@imperial.ac.uk)

6 Manish Sreenivasa<sup>a</sup> - [manishs@uow.edu.au](mailto:manishs@uow.edu.au)

7 <sup>a</sup> School of Mechanical, Materials, Mechatronic and Biomedical Engineering, University of  
8 Wollongong, Northfields Avenue, Wollongong, NSW, 2522, Australia

9 <sup>b</sup> Sackler MSk Laboratory, Department of Surgery and Cancer, Sir Michael Uren Hub, Imperial College  
10 London, 86 Wood Ln, London W12 0BZ, United Kingdom

11

12

13 **Abstract:**

14 This study aimed to investigate normal and shear load sensor technology that has been  
15 characterised and used at the human-device interface in prosthetic, orthotic and exoskeleton  
16 applications. In addition to taking a cross-disciplinary view, this study expands on previous reviews  
17 by considering recently published papers, clinical translation of sensors, and development of the  
18 sensor technology itself. A search of MEDLINE, INSPEC, SCOPUS and Web of Science was performed  
19 up to 26 January 2021. A total of 33 studies were assessed for quality and their data extracted. The  
20 review found variable quality of published papers, with normal load being most commonly  
21 measured, and resistive sensor technology most commonly used. The translation to clinical  
22 environments was indicated in most studies, though the study population was not always made up  
23 of the target users. Studies could benefit from more direct comparison with clinically relevant load  
24 thresholds and by ensuring clinical testing is performed in the most realistic and representative way  
25 possible. Additionally, more focus on developing sensors that measure shear loads would enable  
26 further insights into conditions at the human-device interface. Finally, all researchers would benefit  
27 from better and more widespread anonymous data sharing practices to facilitate further  
28 experimentation.

29 This research did not receive any specific grant from funding agencies in the public, commercial, or  
30 not-for-profit sectors.

31

32 **Background:**

33 Several categories of external medical devices are used to support or replace parts of the body that  
34 are not functioning effectively. In a general sense, prosthetics replace function, orthotics support  
35 function and exoskeletons can support or augment function. The interface between humans and  
36 wearable medical devices is important for the long-term suitability of devices and should minimise  
37 the risk of damage to the underlying anatomical structures and maximise comfort [1]. A device that  
38 is uncomfortable or ill-fitting risks further medical complications, or alters natural loading patterns  
39 that may in turn limit compliance with the device and cause other long-term health issues [2–7].

40 Although the prosthetics, orthotics and exoskeleton research and application fields are generally  
41 distinct, the mechanical state of the interfaces is similar, thus yielding similar clinical implications.

42 A number of literature reviews have been performed over the last decade summarising existing  
43 sensing technology, albeit with a limited focus on prosthetic applications [8–11]. The last of these  
44 occurred 5 years ago, and since then several emerging technologies have been presented in  
45 literature. With the rapid development of orthotic and exoskeleton technology in recent years, there  
46 is a lack of studies that synthesise pressure measurement in orthotic applications or include human-  
47 exoskeleton interfaces. This information will provide an important addition to the current body of  
48 knowledge given the similarity of the mechanical state of the interfaces, with the potential for cross-  
49 disciplinary application of knowledge and technology. In particular, quantitative information about  
50 the interfaces is useful for understanding the clinical relevance of findings, especially if related to  
51 thresholds of clinical importance, e.g. the load at which skin breakdown starts. The current review  
52 then addresses this gap in literature by adopting a cross-sectional view, covering pressure sensing at  
53 the human-device interface in prosthetics, orthotics and exoskeletons. A particular focus is on  
54 studies that show potential for clinical application in relevant experimental tests, and evaluating the  
55 clinical translation of such technologies, both in terms of relevant clinical thresholds and the  
56 technologies themselves.

57 Various load metrics have been used in literature. Forces, measured in Newtons (N) either  
58 perpendicular to or parallel with the surface of interest are commonly measured as normal or shear  
59 forces, respectively. Pressure or stress, defined as force per unit area, is also a common metric and  
60 can also be quantified in the normal or shear directions. Both normal and shear forces are important  
61 to consider in the interface environment due to their potential negative consequences, however,  
62 there is a consensus that shear forces (often due to friction) are the greatest contributor to skin  
63 breakdown [5,12,13]. For the purpose of this review, *load* is used as a blanket term to describe both  
64 force and stress metrics. Where relevant, force or stress will be referred to directly.

65 There are several critical contributing factors to the maintenance of long-term health when using  
66 these devices, in particular, normal and shear forces, moisture and temperature [14] are important  
67 for maintaining skin health. Despite the importance of these factors, literature does little to highlight  
68 the clinical relevance of these quantitative measures, demonstrated by a lack of standard clinical  
69 threshold values. As the devices work by transmitting forces to the body, the location of these load  
70 points on the underlying anatomy is also important. Mechanical load or stress, both normal and  
71 shear, between the user and the device can be the most difficult to adapt to, as only specific parts of  
72 the human anatomy have evolved to bear sustained high loads, e.g. the uncut distal surfaces of the  
73 femur, the calcaneal fat pad on the heel. Most soft tissue, which often serves as the body's interface  
74 with wearable medical devices, is not accustomed to high stress. Skin breakdown and pressure sores  
75 are therefore not uncommon when skin is subjected to pressure [15]. Understanding the mechanics  
76 of the interaction between the human and the device is a major ongoing challenge in these areas of  
77 research [11].

78 Sensing technology may be utilised to effectively monitor the environment at the interface of the  
79 body and an external medical device. The use of sensors to measure normal and shear load can  
80 provide information that would not otherwise be available about the interface. Areas of high stress  
81 can be identified, allowing for the potential avoidance of skin damage in these regions. The

82 quantitative understanding of stress at the device-human interface may allow for further insight into  
83 one of the factors that cause negative consequences for individuals. The information could be used  
84 to determine clear thresholds across cohorts or individuals. Combined with user and clinician  
85 feedback, the quantitative data may be used to enhance clinical decision making. Measuring the  
86 stress at device-human interface sites also provides the means to gain a better understanding of the  
87 relationship between stress, sensation at the interface, and control of active systems that the user is  
88 wearing. Understanding these stresses could allow for a proactive design approach, combined with  
89 everyday monitoring, where modification could occur before users develop issues, and can give an  
90 indication of the threshold above which discomfort or damage is likely. To incorporate the value of  
91 stress measurement into clinical practice, first the clinical utility and value of the technology must be  
92 established. The technologies should be validated and tested in the clinical environment. This will be  
93 the focus area of this review. Subsequent engagement with feedback from clinicians and service  
94 users to optimise technology must then be pursued. Priorities may differ between the research and  
95 clinical perspectives, and acceptability criteria should be established to inform technology  
96 development. Applications outside the clinic may also be considered, opening opportunities for  
97 longer term remote and daily monitoring of loads as well as user health self-management.

98 The measurement of load at the interface between a user and a prosthetic, orthotic or exoskeleton  
99 is typically limited by the need for a low profile, safety and reliability. Factors such as temperature  
100 variation at the interface, curved surfaces and large ranges of loading add further complexity [9].

101 Commercially available load sensors are available as pads for multi-application use, with some  
102 developed for specific applications (e.g. prosthetic sockets, insoles). Commercial options are typically  
103 associated with high costs, restricted software compatibility and minimal information about their  
104 detailed structure. It is in this context that the ongoing development and reporting of sensor  
105 systems for this application occurs.

106 There is also no one definitive technology that has been developed to meet the diverse needs of  
107 researchers and users within or across prosthetics, orthotics and exoskeleton applications.  
108 Therefore, there is ongoing research into custom made sensor systems for specific use in these  
109 fields. Much of the published research is focused on sensor development and property  
110 characterisation through benchtop testing, with little demonstration of use in the intended  
111 application. For instance, Armitage et al. have described the fabrication and bench testing process of  
112 a normal and shear fiber Bragg grating sensor system, embedded in a prosthetic liner material,  
113 however, no testing with either residual limb models nor human participants has been reported in  
114 the study [16]. This makes it difficult for others to infer whether they will be appropriate for use  
115 clinically without the need for a larger scale clinical study.

116 An alternative to a large-scale clinical study is to present preliminary results based on a few  
117 participants, with the main purpose being to bridge the gap between benchtop testing and the  
118 clinical implementation. Participant testing is important to determine whether the sensors are fit for  
119 their clinical application, the requirements of which vary between applications. It is also important  
120 to demonstrate that the sensors add value to the clinical application being targeted. The gap  
121 between benchtop testing and clinical application should be minimised to ensure the technologies  
122 developed add the intended value. Ideally, the technology would be designed in collaboration with  
123 end users, both clinicians and device users, to minimise wasted resources and to achieve the  
124 required results.

125 The stage of development between benchtop testing and preliminary assessment of the device in  
126 the clinic will be the focus of this study. We seek to identify methods and technologies in the  
127 literature that will assist researchers in taking promising technology from the laboratory into the  
128 clinic.

129 This review focuses on translational studies of normal and shear load sensor technology that have  
130 been developed, characterised and used in preliminary clinical assessment at the human-device



131 interface in regions of the body that do not usually bear loads. Plantar pressure measurement was  
132 excluded from this review as we deemed the foot a region of usual load bearing, and there is a  
133 significant body of literature and reviews pertaining directly to this type of pressure measurement  
134 already.

135 This study has three aims. Firstly, to understand and report how interface pressure is currently  
136 measured in prosthetic, orthotic and exoskeleton applications. Secondly, to evaluate the methods  
137 used for clinical translation of the technologies in terms of testing and performance. Finally, to  
138 assess the quality of the reporting of these studies with a view to providing authors with guidance  
139 on improving the quality of the overall body of knowledge available to the community.

#### 140 **Methods:**

##### 141 *Study selection*

142 The protocol of this systematic review was registered with PROSPERO (registration number  
143 CRD42020181809). Methods have been developed and presented in line with the Preferred  
144 Reporting Items for Systematic Reviews and Meta-Analyses (PRISMA) guidelines [17]. Studies that  
145 investigated the use of load (normal or shear) sensors at an interface between a human or limb  
146 model or phantom, that does not usually bear loads, and a prosthetic, orthotic or exoskeleton device  
147 were considered. Only journal articles published in English were included. A full list of inclusion and  
148 exclusion criteria is available in Appendix 1.

##### 149 *Data Sources and Search*

150 A search strategy for MEDLINE, Web of Science, Inspec and Scopus was developed in consultation  
151 with a librarian at the XXXX. The search strategies have been included in Appendix 2. The databases  
152 were searched up until 26 January 2021. 2 assessors (L.A. and M.S.) independently screened titles  
153 and abstracts for eligibility, followed by full text articles. Personal libraries and reference lists of  
154 included studies were also screened for relevant articles. Any discrepancies between selections were

155 resolved via discussion between assessors and where necessary, the involvement of a third assessor  
156 (S.T.).

#### 157 *Data Extraction*

158 2 assessors (L.A. and S.T) independently extracted study characteristics using standardised forms.  
159 These data included study aims, application field, sensor type, range, number and locations,  
160 validation or calibration procedures, experimental protocols, and pressure thresholds for clinical  
161 significance. A full list of the items collected has been included in Appendix 3. These items were  
162 included as they provide useful guidance to other researchers as to the experimental protocols for  
163 interface sensor testing.

#### 164 *Quality Assessment*

165 There are several existing quality rating scales with items relevant to our study [18–21], however, no  
166 single quality rating scale previously used in the literature covered all items we wished to assess in  
167 this review. For example: items pertaining directly to sensor calibration are not routinely included in  
168 clinical studies, and items referring to the diagnostic ability of clinical tools are not relevant to our  
169 study. Therefore, a combination of the items used in the other reviews was developed. It included  
170 items pertaining to reporting of aims, methods, limitations and conclusions, characteristics of the  
171 anatomical landmarks, sensor configuration, sample size and demographic, usage of appropriate  
172 statistical analysis, availability of raw data and comparison to existing clinical data. Each item was  
173 scored with 'Yes' = 2, 'Unclear' = 1 or 'No' = 0. All items were equally weighted, and the total score  
174 was calculated across 13 items to give a total out of 26. Studies were considered high quality if they  
175 achieved a score of 17/26 or higher, moderate quality if they achieved a score between 9/26 and  
176 less than 17/26 and low quality if they achieved a score of less than 9/26. Prior to completing the  
177 quality assessment, 3 assessors attended a quality rating scale training session to ensure fairness of  
178 assessment. 2 assessors (S.T. and M.S) then independently completed the quality assessment.  
179 Where discrepancies were present, a third assessor (L.A.) assisted in resolution.

180 **Results:**

181 *Eligible studies*

182 An initial search was performed on 5 June 2020 and resulted in 11501 articles being identified. After  
183 removal of duplicates 8316 remained. Title and abstract screening removed 8280 articles that did  
184 not meet the inclusion criteria. 36 full text articles were screened, from which a further 7 were  
185 excluded. A final re-run of the search was performed on 26 January 2021 which resulted in an  
186 additional 1175 titles and abstracts from June 2020 and January 2021. After screening and removal  
187 of duplicates 797 remained. From this group, an additional 5 relevant papers were identified and  
188 included.

189 At the end, a total of 33 articles were included in the review, of which 17 pertained to prosthetic  
190 devices, 7 to orthotic devices and 9 to exoskeletons. A PRISMA flowchart presenting the total  
191 number of studies at each stage has been included in Figure 1 and an outline of general study  
192 characteristics is included in Table 1.

193 [Insert Figure 1 here]

194

195 [Insert Table 1 here]

196 *Data extraction*

197 *Interface Stress Measurement*

198 Data were extracted from 17 prosthetic studies [22–38], 7 orthotic studies [39–45] and 9  
199 exoskeleton studies [46–54], with the characteristics summarised in Table 1 and results summarised  
200 in Table 2. Prosthetics studies included sample sizes from 1 to 4 with a total of 23 participants (Table  
201 1). 3 of the prosthetic studies also used limb phantoms instead of human subjects. Orthotics studies  
202 included sample sizes ranging from 1 to 44, with a total of 110 participants (Table 1). Studies  
203 pertaining to exoskeletons included sample sizes ranging from 1-8 with a total of 29 participants  
204 (Table 1).

205 The most popular sensor types used in the studies across the 3 application areas were resistive (11  
206 studies). Fiber Bragg Grating technology (5 studies) was also explored in prosthetic and exoskeleton  
207 applications (Item 2, Table 2). Normal force or stress was the dominant type of load that was  
208 measured (28 studies) (Item 3, Table 2).

209 *Clinical Translation*

210 Parameters relating to clinical translation included anatomical locations of sensors, testing on  
211 human subjects rather than phantoms only, the types of movements measured and the inclusion of  
212 clinical thresholds with respect to safe loads.

213 There was a wide range of approaches with respect to the location of sensors, with some studies  
214 measuring at specific anatomical points, particularly in exoskeleton (9 studies) and prosthetic  
215 applications (14 studies). Others, predominantly orthotic applications (6 studies), used large surface  
216 pressure measurements systems across the whole interface (Item 4, Table 2). Prosthetic applications  
217 saw the most diversity in the number and location of sensors. Lower limbs and locations on the  
218 trunk were most common, with only 4 studies investigating interface stress on the upper limb (Item

219 5, Table 2). Sensors were designed with a variety of normal and shear force or pressure ranges  
220 (Items 6 and 7, Table 2). 31 studies outlined their calibration process in the paper (Item 8, Table 2).  
221 31 studies performed their translational testing on human subjects rather than phantoms (Item 9,  
222 Table 2). As a result of the large number of studies on human subjects, a broad range of human  
223 movements were examined (Item 10, Table 2). Of note when considering translation of this  
224 technology into a clinical setting is the ability for functional movements to be performed without  
225 restriction. In the context of lower limb devices, 22 studies reported data related to walking, 2 with  
226 respect to turning and 1 with respect to stairs. This would suggest these devices are portable, which  
227 is an important feature if longer term monitoring in daily life is also a consideration. Inferences  
228 about the portability of devices used for movements not involving ambulation were not made.

229 Nine studies reported clinical thresholds with respect to safe loads and used these to compare to  
230 their data (Item 11, Table 2). Clinical load thresholds used in the exoskeleton papers included a  
231 general reference to various pain pressure thresholds [47,50]. We noted that studies used 4.7 kPa  
232 for the onset of ischaemia [49], 40-50 mmHg (5.3 - 6.7 kPa) for tissue oxygenation and 30-35 mmHg  
233 (4 – 4.7 kPa) for adequate circulation [52]. There was also reference to the graphical representation  
234 of thresholds with different durations of exposure [54]. Pressure thresholds used as references in  
235 the orthotics papers included 40-60 mmHg for pressure sores [43]. Clinical thresholds that were used  
236 as references in the prosthetics papers included 8 kPa for ischaemia [22], pressures greater than 100  
237 kPa potentially being dangerous [23] and pressures greater than 20 kPa leading to prosthetic  
238 tightness [29].

239 [Insert Table 2 here]

#### 240 *Quality Assessment*

241 The quality assessment of the papers has been summarised in Table 3. 17 of the studies were  
242 considered to be of high quality [22,25,26,32–38,40,42–44,50,52,54], 13 of moderate quality [23,27–

243 31,39,45–48,51,53], and 3 of low quality [24,41,49]. Of the 9 exoskeleton papers, 3 were rated as  
244 high quality, 5 as moderate and 1 as low. Of the 7 orthotic papers, 4 were rated as high quality, 2  
245 and moderate and 1 as low. Of the 17 prosthetics papers, 10 were rated as high quality, 6 as  
246 moderate and 1 as low.

247 Most studies provided good information on aims, participant details, findings and conclusions and  
248 included measurements from all participants. Common limitations included lack of detailed  
249 information about the interface where the sensor was acting; and lack of details about sample size  
250 calculations and statistical measures, if they were performed. There was also limited comparison of  
251 results to existing pressure or shear stress benchmarks in the literature. Only 1 study provided  
252 access to raw or processed data [38]. Figure 2 shows the breakdown of scores by item for each  
253 application area.

254 [Insert Table 3 here]

255 [Insert Figure 2 here]

256

257 **Discussion:**

258 The results of this review showcase an inter-disciplinary approach to measuring interface pressure  
259 across prosthetic, orthotic and exoskeleton applications. Existing technologies have been identified  
260 through a systematic review with a focus on studies providing initial clinical translation of the  
261 technologies, demonstrating both sensor development and the direct application of the sensors on  
262 human participants or phantoms. It is important to note that the review did not distinguish whether  
263 the studies were implemented in a clinical setting (i.e. hospital or practice). Rather, the definition of  
264 translation to a clinical environment focused on the use of the sensor system in an experiment that  
265 mirrored conditions that may occur in the clinic. This was a necessary distinction to make as the  
266 review focused on studies that documented the translation from non-clinical benchtop tests to  
267 preliminary human or phantom testing rather than studies implementing existing sensor systems in  
268 a clinical study.

269 It is significant that, despite a stringent exclusion criterion, 33 recent studies were identified that  
270 went beyond benchtop testing and achieved some aspect of the translation to clinical environments  
271 by completing initial testing with target users or on a limb phantom. As a vital step towards full  
272 clinical testing, these efforts should be acknowledged. However, we also noted several avenues for  
273 improvement across the studies. In the following we discuss our findings with the perspective to find  
274 synergies between approaches used in prosthetic, orthotic and exoskeleton research, as well as  
275 common challenges.

276 *Data extraction*

277 The majority of studies examined aimed to determine an absolute load that may be applied at a  
278 desired location. The nature of the device, particularly its flexibility and shape (e.g. curvature), are  
279 known to impact its characterisation and consequently the measured values. While some  
280 characterisation protocols do account for the effect of curvature or calibrate the sensors in situ, the  
281 flexibility of the material was not typically discussed. It is therefore likely that for more flexible

282 surfaces, e.g. the prosthetic socket or hand orthoses, relative rather than absolute pressure was  
283 being recorded.

284 Assessment of the diverse sensor technologies investigated in the reviewed studies found no  
285 definitive system that clearly outperformed others across applications. In many of the studies, there  
286 was a clear focus on normal rather than shear load measurement. However, it is important to note  
287 that shear loading is thought to be responsible for 40% of pressure ulcers [55]. While some state-of-  
288 the-art systems are beginning to address simultaneous normal and shear measurement (e.g. [56]) ,  
289 our results clearly indicate that further research and development of shear sensing technology is  
290 needed [11,57]. As the true loading state is made up of combined normal and shear load,  
291 development of sensors capable of measuring both types of stress simultaneously would be ideal.

292 There was substantial variation in the values used as clinical indications for pressure tolerance. This  
293 is not a negative finding, as it is likely that different anatomical landmarks and applications have  
294 different requirements [52,58]. It does, however, highlight a general lack of consensus in the  
295 literature as to 'safe' thresholds for interface loads when using these devices. Furthermore, a key  
296 aspect of user acceptance of an external device is the perception of comfort, a subjective metric that  
297 a sensor will not be able to measure. Our appraisal of the studies in this review suggests that it is  
298 unlikely that sensors and load recordings alone could be an effective tool to assess the suitability of  
299 use of a sensor system in a given device or of the device itself. Therefore, the use of sensor  
300 technology in studies would benefit from correlations between the objective pressure readings and  
301 user and clinician preferences. This is a potential area of future research for the sensors systems that  
302 have high quality studies to back up their use. This research may also benefit from borrowing  
303 methods and approaches used in ergonomics (e.g. [59]) and modelling (e.g. [60]).

304 A particularly encouraging finding from this review was that the majority of studies used human  
305 subjects to perform preliminary testing. It should be acknowledged that it is challenging to replicate  
306 the complex loading state at the human-device interface with a phantom, which may affect sensor



307 performance. Most studies employed sensors at discrete anatomical landmarks rather than  
308 instrumenting the entire interface. This was perhaps due to the translational nature of the work,  
309 where authors were testing feasibility at discrete points before developing more complex networks  
310 to measure over larger areas. It may also indicate that the clinical focus in these applications tends  
311 to be towards ‘trouble areas’ where discrete stress measurement is adequate. Regardless, there  
312 were several high and moderate quality studies that support either approach, with orthotics  
313 applications tending to favour large area pressure mapping and prosthetic and exoskeleton  
314 applications focusing on discrete points.

### 315 *Quality assessment*

316 No trends were identified in the study quality across different types of sensors or for the application  
317 areas (i.e. prosthetics, orthotics, exoskeletons). The quality of the studies was mixed across these  
318 categories, with the majority of studies being of moderate or high quality. The lowest scored  
319 category across all disciplines was the provision of raw data by authors from their conducted  
320 experiments. This was particularly discouraging considering the easy availability of free online data  
321 repositories such as GitHub, Zenodo etc., some of which also allow for tagging datasets with DOIs  
322 (thus allowing formal acknowledgement of data re-use and improving citation counts). Of the 33  
323 papers reviewed, only 1 prosthetics paper published their raw data for readers to access [38]. The  
324 availability of anonymised raw data is good practice as it allows readers to understand the  
325 conclusions made and perform analyses themselves to replicate and extend the methods. The  
326 publication of the raw data also allows the amalgamation of data sets which could lead to more  
327 robust investigations, particularly beneficial for areas with low participation numbers.

328 There was a relatively even distribution of study quality across different sensor types. The highest  
329 numbers of moderate and high quality studies covered resistive sensors, Fiber Bragg gratings and  
330 strain gauges. This does not exclude the merit of the other technologies that were explored, but  
331 highlights the need for further studies to provide more robust evidence for use.

332 We noted a particular lack of reporting of clinically relevant thresholds for acceptable load levels,  
333 either normal or shear. While this can make it difficult to understand whether the measured levels  
334 of load in the studies pose a clinical problem, it is not an unexpected omission. Literature has  
335 reported various acceptable load thresholds, with no specific range universally accepted [58,61]. The  
336 acceptable levels of load vary across the body of an individual, and across different individuals. It  
337 may also significantly vary with the size of the interface and the duration of the loading. Many of the  
338 papers included in the review do not outline the assessment of acceptable pressure in clinical  
339 applications as an aim, rather they outlined the manufacture and testing of the sensor technologies  
340 to understand if they were fit for purpose. Future research using the technologies outlined in the  
341 included studies would be beneficial to evaluate the clinical relevance of the sensor devices.

342 The translation from sensor fabrication and characterisation to clinical use is a vital step in the  
343 successful integration of new technology into the clinic. Studies demonstrating the details required  
344 for clinicians to select, build, calibrate and run published technology open opportunities for  
345 increased clinical use in similar and different contexts.

346 Strength of conclusions was a particular issue when studies did not include many participants, or the  
347 tests were conducted on a convenient population (e.g. healthy adults, male) rather than the target  
348 demographic of the technology. Sample size was generally small, with only a few papers explicitly  
349 stating that they were conducting preliminary or pilot testing. It was noteworthy that in some  
350 instances, none of the participants tested were representative of the intended end users, and yet  
351 conclusions were drawn about the suitability of the technology for them. Based on the review, we  
352 would encourage authors to consider highlighting the next steps required to continue to ensure  
353 technology is fit for purpose in the specific demographic.

354 Based on titles and abstracts that were reviewed but not included in this study, it was common for  
355 studies to report that newly developed sensors were appropriate for use in a clinical context without  
356 including any data on clinical testing having been performed. In order to ensure that the most

357 clinically and technically appropriate sensors can be selected for a specific application, it would be  
358 highly beneficial that the additional steps of including details of preliminary clinical testing and  
359 experimental protocols are taken, and that it is demonstrated that the technology is fit for purpose.  
360 This review selected papers positioned between the traditional benchtop and full clinical testing. As  
361 a result, sample sizes were generally smaller, and focused on showing the feasibility of the sensor  
362 systems rather than answering clinical questions. This also meant that statistical measures were not  
363 widely utilised. Studies were also generally completed in a laboratory. Therefore, it is important to  
364 note that the conclusions about the studies here will not necessarily apply to studies conducting  
365 more robust clinical testing. Rather, the purpose is to provide authors with some guidance on  
366 pertinent reporting guidance for studies that fit in this context and summarise existing technology  
367 that may lead to innovation across disciplines. It is clear that once a sensor has been deemed fit for  
368 purpose, the next steps would involve the move to formal clinical testing. If the aim is to determine  
369 pressure tolerance or a particular pressure distribution for individuals in activities of daily living, a  
370 relative pressure reading may be adequate with testing in the home environment instead of the  
371 laboratory or clinic. However, if trends and comparisons are sought for multiple users, relative  
372 pressure may be too subjective. Further development and testing of the sensors may be required to  
373 characterise sensors in wider applications to minimise the error of absolute values and ensure  
374 robust readings for comparison. The questions to be answered should be directed by those who use  
375 and fit the devices; collaboration with relevant clinicians, device users and researchers should be at  
376 the centre of determining the appropriate use of the sensors and future testing to allow for robust  
377 interpretation of values. Another aspect of development is the ease of use in the desired  
378 environment, with development of user interfaces and fabrication methods to allow this and quick  
379 interpretation of values without the need for engineering specific expertise.

380 *Considerations for Clinical Translation*

381 Clinical use for sensor systems may be broadly divided into use at the time of device fitting, i.e. in  
382 the clinic, with a health professional, and, secondly, for longer term monitoring of loads during  
383 normal daily life, i.e. outside the clinic, in the community. Deciding whether a particular sensor  
384 system is appropriate for use in a given application requires consideration of a combination of  
385 parameters reported in the data extraction section (for example pressure range of interest and  
386 anatomical location) as well as parameters reported in the quality rating of the study (for example,  
387 whether the sensors are validated, and whether there was enough information reported to allow  
388 the system to be implemented effectively). Considerations such as portability of the device for  
389 applications where participants need to move around, or ensuring that the prosthesis, orthosis or  
390 exoskeleton does not need to be permanently modified to integrate sensors will also be relevant  
391 depending on the application. In thinking about further translation into systems to be used for  
392 longer term monitoring outside the clinic, considerations such as portability, data recording and  
393 security and power requirements, user comfort and preference are also essential.

394 The studies included in the review did not explore further possibilities for clinical translation,  
395 including seeking feedback from users (clinicians and service users) on preferences for the  
396 technologies or how they could be used to complement routine practice. There was also no  
397 indication that the application of the sensors would be modified for ease of use without specialised  
398 engineering knowledge. For instance, it has been demonstrated that various sensors including,  
399 temperature, pressure, shear and humidity sensors can be incorporated into a wearable devices,  
400 such as a prosthetic liner [62,63]. The advantage here is the relative ease of use in the clinical  
401 environment, which makes it suitable for application without need for specialist knowledge of the  
402 technology. Additional studies (not included in the current review due to the inclusion criteria)  
403 complete testing with service users using commercial sensor technologies; Tekscan sensors, in  
404 particular, are a frequently used product in this context [64–66].

405 It is also important to consider how the information from the sensing technologies is going to be  
406 understood by clinicians and service users, a crucial part of ensuring the hardware adds value to the

407 clinical environment. Software development can be an asset for this, with the creation of an easy-to-  
408 understand user interface making complex technologies and extensive data comprehensible and  
409 useful. This has been demonstrated in previous studies, both with and without the use of sensors to  
410 inform data presented [67–69].

411 Due to the translational nature of the reported studies, a vital aspect of clinical translation was  
412 missing: i.e. the engagement with the end-users, both the clinicians and users of the devices.

413 From the methods outlined in the reviewed studies, whilst some indicated awareness of clinical  
414 issues (e.g. the need for stress monitoring or clinical thresholds), most did not integrate feedback  
415 from target users. This presents an exciting area for future work.

416

#### 417 **Study limitations**

418 Our review focused on a subset of studies within the identified application areas, and can be  
419 associated with the following limitations. First, studies not published in English were not considered.  
420 Second, we only included peer reviewed journal articles. By excluding conference proceedings, we  
421 may have overlooked initial translational research that tends to get published in the relative faster  
422 review process associated with conferences. Third, the reliability and validity of the quality rating  
423 scale was not assessed. Although every attempt was made to develop the scale based on established  
424 quality rating scales, consistency of interpretation of the scale and studies by researchers outside of  
425 the study have not been performed. Finally, studies included in this review needed to include both  
426 sensor development and benchtop calibration as well as preliminary clinical tests to meet the  
427 inclusion criteria. This meant that any studies detailing only sensor development or only clinical  
428 testing have not been included. It is also worth noting that as a field of ongoing research, new  
429 technologies and solutions are being constantly developed. For example, the recent study by Deijke  
430 et al. [63] showcases relevant pressure sensor technology for prosthetic applications. However, this

431 study was published after the inclusion period specified for our current review and hence not  
432 included in the results.

433

434 In summary, the results of the review showed that the quality of papers in the prosthetic, orthotic  
435 and exoskeleton areas was variable. While different sensing technologies were tested across the  
436 disciplines, there was no one accepted as universally appropriate. The measurement of normal load  
437 was more common than shear despite it being accepted as a key factor in comfort and skin  
438 breakdown. Most studies started the process of understanding the acceptability of translating the  
439 sensing technologies into the clinical environment by conducting some initial testing with a study  
440 population, with some also comparing their results to significant clinical thresholds. However, study  
441 populations were generally small and were not always made up for the target users and reported  
442 clinical thresholds were not consistent. In general, studies could be strengthened by performing  
443 clinical testing with target populations in relevant environments and shared progress and  
444 understanding could be achieved by sharing de-identified data.

445

#### 446 **Acknowledgments**

447 Associate Professor Lauren Kark, Graduate School of Biomedical Engineering, UNSW Australia

448 Christine Wales, Librarian, University of Wollongong

449

450 Competing interests: Author ST works in the same laboratory as the authors listed on one of the  
451 reviewed papers, although was not involved in any way in the study that was reviewed.

452 Funding: None

453 Ethical approval: Not required

454

455

456

457 **References**

- 458 [1] Turner S, McGregor AH. Perceived Effect of Socket Fit on Major Lower Limb Prosthetic  
459 Rehabilitation: A Clinician and Amputee Perspective. *Arch Rehabil Res Clin Transl*  
460 2020;2:100059. [https://doi.org/https://doi.org/10.1016/j.arrct.2020.100059](https://doi.org/10.1016/j.arrct.2020.100059).
- 461 [2] Farrokhi S, Mazzone B, Eskridge S, Shannon K, Hill OT. Incidence of Overuse Musculoskeletal  
462 Injuries in Military Service Members With Traumatic Lower Limb Amputation. *Arch Phys Med*  
463 *Rehabil* 2018;99:348-354 e1. <https://doi.org/10.1016/j.apmr.2017.10.010>.
- 464 [3] Levy SW. Skin problems of the leg amputee. *Prosthet Orthot Int* 1980;4:37–44.  
465 <https://doi.org/10.3109/03093648009103113>.
- 466 [4] Gailey R, Allen K, Castles J, Kucharik J, Roeder M. Review of secondary physical conditions  
467 associated with lower-limb amputation and long-term prosthesis use. *J Rehabil Res Dev*  
468 2008;45:15–29. <https://doi.org/10.1682/Jrrd.2006.11.0147>.
- 469 [5] Meulenbelt HE, Geertzen JH, Dijkstra PU, Jonkman MF. Skin problems in lower limb  
470 amputees: an overview by case reports. *J Eur Acad Dermatol Venereol* 2007;21:147–55.  
471 <https://doi.org/10.1111/j.1468-3083.2006.01936.x>.
- 472 [6] Rocon E, Pons JL. Exoskeletons in rehabilitation robotics: Tremor suppression. vol. 69.  
473 Springer; 2011.
- 474 [7] Xiloyannis M, Chiaradia D, Frisoli A, Masia L. Physiological and kinematic effects of a soft  
475 exosuit on arm movements. *J Neuroeng Rehabil* 2019;16:29. [https://doi.org/10.1186/s12984-](https://doi.org/10.1186/s12984-019-0495-y)  
476 [019-0495-y](https://doi.org/10.1186/s12984-019-0495-y).
- 477 [8] Silver-Thorn MB, Steege JW, Childress DS. A review of prosthetic interface stress  
478 investigations. *J Rehabil Res Dev* 1996;33:253–66.



- 479 [9] Al-Fakih AE, Abu Osman AN, Mahmad Adikan RF. Techniques for Interface Stress  
480 Measurements within Prosthetic Sockets of Transtibial Amputees: A Review of the Past 50  
481 Years of Research. *Sensors* 2016;16. <https://doi.org/10.3390/s16071119>.
- 482 [10] Pirouzi G, Osman NAA, Eshraghi A, Ali S, Gholizadeh H, Abas WABW. Review of the Socket  
483 Design and Interface Pressure Measurement for Transtibial Prosthesis 2014;2014.
- 484 [11] Safari R. Lower limb prosthetic interfaces: Clinical and technological advancement and  
485 potential future direction. *Prosthet Orthot Int* 2020;44:384–401.  
486 <https://doi.org/10.1177/0309364620969226>.
- 487 [12] Highsmith JT, Highsmith MJ. Common skin pathology in LE prosthesis users. *JAAPA*  
488 2007;20:33–7. <https://doi.org/10.1097/01720610-200711010-00017>.
- 489 [13] NAYLOR PFD. Experimental Friction Blisters. *Br J Dermatol* 1955;67:327–42.  
490 <https://doi.org/10.1111/j.1365-2133.1955.tb12657.x>.
- 491 [14] Paterno L, Ibrahimi M, Gruppioni E, Menciassi A, Ricotti L. Sockets for Limb Prostheses: A  
492 Review of Existing Technologies and Open Challenges. *IEEE Trans Biomed Eng* 2018;65:1996–  
493 2010. <https://doi.org/10.1109/TBME.2017.2775100>.
- 494 [15] Bouten C V, Oomens CW, Baaijens FP, Bader DL. The etiology of pressure ulcers: skin deep or  
495 muscle bound? *Arch Phys Med Rehabil* 2003;84:616–9.  
496 <https://doi.org/10.1053/apmr.2003.50038>.
- 497 [16] Armitage L, Rajan G, Kark L, Simmons A, Prusty BG. Simultaneous measurement of normal  
498 and shear stress using fiber bragg grating sensors in prosthetic applications. *IEEE Sens J*  
499 2019;19:7383–90. <https://doi.org/10.1109/JSEN.2019.2914702>.
- 500 [17] Moher D, Liberati A, Tetzlaff J, Altman DG. Research methodes and reporting. *Bmj*  
501 2009;8:332–6.

- 502 [18] Vandembroucke JP, von Elm E, Altman DG, Gøtzsche PC, Mulrow CD, Pocock SJ, et al.  
503 Strengthening the Reporting of Observational Studies in Epidemiology (STROBE): explanation  
504 and elaboration. *Ann Intern Med* 2007;147:W163-94. [https://doi.org/10.7326/0003-4819-](https://doi.org/10.7326/0003-4819-147-8-200710160-00010-w1)  
505 [147-8-200710160-00010-w1](https://doi.org/10.7326/0003-4819-147-8-200710160-00010-w1).
- 506 [19] Deeks JJ. Systematic reviews in health care: Systematic reviews of evaluations of diagnostic  
507 and screening tests. *BMJ* 2001;323:157–62. <https://doi.org/10.1136/bmj.323.7305.157>.
- 508 [20] Oxman AD. Checklists for review articles. *BMJ* 1994;309:648–51.  
509 <https://doi.org/10.1136/bmj.309.6955.648>.
- 510 [21] Cook DJ, Mulrow CD, Haynes RB. Systematic reviews: synthesis of best evidence for clinical  
511 decisions. *Ann Intern Med* 1997;126:376–80. [https://doi.org/10.7326/0003-4819-126-5-](https://doi.org/10.7326/0003-4819-126-5-199703010-00006)  
512 [199703010-00006](https://doi.org/10.7326/0003-4819-126-5-199703010-00006).
- 513 [22] Laszczak P, Mcgrath M, Tang J, Gao J, Jiang L, Bader DL, et al. A pressure and shear sensor  
514 system for stress measurement at lower limb residuum/socket interface. *Med Eng Phys*  
515 2016;38:695–700.
- 516 [23] Convery P, Buis AWP. Conventional patellar-tendon-bearing (PTB) socket/stump interface  
517 dynamic pressure distributions recorded during the prosthetic stance phase of gait of a trans-  
518 tibial amputee. *Prosthet Orthot Int* 1998;22:193–8.  
519 <https://doi.org/10.3109/03093649809164484>.
- 520 [24] Ruda EM, Avile OF, Mauledoux MF. Design of a mechatronic device for measuring stump  
521 stresses on transfemoral amputees. *J Eng Appl Sci* 2018;13:4880–6.  
522 <https://doi.org/10.3923/jeasci.2018.4880.4886>.
- 523 [25] Al-Fakih EA, Osman NAA, Adikan FRM, Eshraghi A, Jahanshahi P. Development and validation  
524 of fiber Bragg grating sensing pad for interface pressure measurements within prosthetic  
525 sockets. *IEEE Sens J* 2015;16:965–74.

- 526 [26] Ko C-Y, Kim SG, Cho YK, Lee D, Kim DH, Ryu J, et al. Development of a sensor to measure  
527 stump/socket interfacial shear stresses in a lower-extremity amputee. *Int J Precis Eng Manuf*  
528 2018;19:899–905.
- 529 [27] Jasni F, Hamzaid NA, Abd Muthalif AG, Zakaria Z, Shasmin HN, Ng S-C. In-socket sensory  
530 system for transfemoral amputees using piezoelectric sensors: An efficacy study. *IEEE/ASME*  
531 *Trans Mechatronics* 2016;21:2466–76.
- 532 [28] Swanson EC, McLean JB, Allyn KJ, Redd CB, Sanders JE. Instrumented socket inserts for  
533 sensing interaction at the limb-socket interface. *Med Eng Phys* 2018;51:111–8.
- 534 [29] Polliack AA, Craig DD, Sieh RC, Landsberger S, McNeal DR. Laboratory and clinical tests of a  
535 prototype pressure sensor for clinical assessment of prosthetic socket fit. *Prosthet Orthot Int*  
536 2002;26:23–34.
- 537 [30] Sanders JE, Daly CH. Measurement of stresses in three orthogonal directions at the residual  
538 limb-prosthetic socket interface. *IEEE Trans Rehabil Eng* 1993;1:79–85.
- 539 [31] Al-Fakih E, Arifin N, Pirouzi G, Mahamd Adikan FR, Shasmin HN, Abu Osman NA. Optical fiber  
540 Bragg grating-instrumented silicone liner for interface pressure measurement within  
541 prosthetic sockets of lower-limb amputees. *J Biomed Opt* 2017;22:1.  
542 <https://doi.org/10.1117/1.jbo.22.8.087001>.
- 543 [32] El-Sayed AM, Hamzaid NA, Abu Osman NA. Piezoelectric bimorphs' characteristics as in-  
544 socket sensors for transfemoral amputees. *Sensors* 2014;14:23724–41.
- 545 [33] Ferreira A, Correia V, Mendes E, Lopes C, Vaz JFV, Lanceros-Mendez S. Piezoresistive polymer-  
546 based materials for real-time assessment of the stump/socket interface pressure in lower  
547 limb amputees. *IEEE Sens J* 2017;17:2182–90.
- 548 [34] Al-Fakih EA, Osman NAA, Eshraghi A, Adikan FRM. The capability of fiber Bragg grating  
549 sensors to measure amputees' trans-tibial stump/socket interface pressures. *Sensors*

550 2013;13:10348–57.

551 [35] Williams RB, Porter D, Roberts VC, Regan JF. Triaxial force transducer for investigating  
552 stresses at the stump/socket interface. *Med Biol Eng Comput* 1992;30:89–96.

553 [36] Ibarra Aguila S, Sánchez GJ, Sauvain EE, Alemon B, Fuentes-Aguilar RQ, Huegel JC. Interface  
554 Pressure System to Compare the Functional Performance of Prosthetic Sockets during the  
555 Gait in People with Trans-Tibial Amputation. *Sensors* 2020;20:7043.

556 [37] Hopkins M, Vaidyanathan R, Mcgregor AH. Examination of the performance characteristics of  
557 velostat as an in-socket pressure sensor. *IEEE Sens J* 2020;20:6992–7000.

558 [38] Kwak JW, Han M, Xie Z, Chung HU, Lee JY, Avila R, et al. Wireless sensors for continuous,  
559 multimodal measurements at the skin interface with lower limb prostheses. *Sci Transl Med*  
560 2020;12.

561 [39] Tan X, He L, Cao J, Chen W, Nanayakkara T. A Soft Pressure Sensor Skin for Hand and Wrist  
562 Orthoses. *IEEE Robot Autom Lett* 2020;5:2192–9.

563 [40] Loukos I, Zachariou C, Nicolopoulos C, Korres D, Efstathopoulos N. Analysis of the corrective  
564 forces exerted by a dynamic derotation brace (DDB). *Prosthet Orthot Int* 2011;35:365–72.

565 [41] Hudák R, Rajtůková V, Živčák J. Automatization of contact pressure measurement between  
566 trunk orthosis and patient’s body using a matrix tactile sensor. *Acta Mech Autom* 2015;9:38–  
567 43.

568 [42] Mac-Thiong J-M, Petit Y, Aubin C-É, Delorme S, Dansereau J, Labelle H. Biomechanical  
569 evaluation of the Boston brace system for the treatment of adolescent idiopathic scoliosis:  
570 relationship between strap tension and brace interface forces. *Spine (Phila Pa 1976)*  
571 2004;29:26–32.

572 [43] Wong MS, Evans JH. Biomechanical evaluation of the Milwaukee brace. *Prosthet Orthot Int*

573 1998;22:54–67.

574 [44] Nowak MD, Abu-Hasaballah KS, Cooper PS. Design enhancement of a solid ankle-foot  
575 orthosis: real-time contact pressures evaluation. *J Rehabil Res Dev* 2000;37:273–81.

576 [45] Kadhim FM, Awad SF, Al-Din Tahir MS. Design and Manufacturing of Portable Pressure Sensor  
577 for Measuring the Interface Pressure between the Body and (Orthosis or Socket Prosthesis). *J.*  
578 *Biomimetics, Biomater. Biomed. Eng.*, vol. 45, Trans Tech Publ; 2020, p. 12–21.

579 [46] Donati M, Vitiello N, De Rossi SMM, Lenzi T, Crea S, Persichetti A, et al. A flexible sensor  
580 technology for the distributed measurement of interaction pressure. *Sensors* 2013;13:1021–  
581 45.

582 [47] Wang Y, Qiu J, Cheng H, Zheng X. Analysis of Human–Exoskeleton System Interaction for  
583 Ergonomic Design. *Hum Factors* 2020:0018720820913789.

584 [48] Leal-Junior A, Theodosiou A, Díaz C, Marques C, Pontes MJ, Kalli K, et al. Fiber Bragg Gratings  
585 in CYTOP Fibers Embedded in a 3D-Printed Flexible Support for Assessment of Human–Robot  
586 Interaction Forces. *Materials (Basel)* 2018;11:2305.

587 [49] Herrán J, Fernández I, Ochoteco E, Cabañero G, Grande H, Moreno JC, et al. Flexible and large  
588 area pressure sensors for human-neuroprostheses and human-neurorobotic interface  
589 assessment. *Microsyst Technol* 2012;18:1155–61.

590 [50] Lenzi T, Vitiello N, De Rossi SMM, Persichetti A, Giovacchini F, Roccella S, et al. Measuring  
591 human–robot interaction on wearable robots: A distributed approach. *Mechatronics*  
592 2011;21:1123–31.

593 [51] Leal-Junior AG, Díaz CR, Pontes MJ, Marques C, Frizera A. Polymer optical fiber-embedded,  
594 3D-printed instrumented support for microclimate and human-robot interaction forces  
595 assessment. *Opt Laser Technol* 2019;112:323–31.

- 596 [52] Tamez-Duque J, Cobian-Ugalde R, Kilicarslan A, Venkatakrisnan A, Soto R, Contreras-Vidal JL.  
597 Real-time strap pressure sensor system for powered exoskeletons. *Sensors* 2015;15:4550–63.
- 598 [53] De Rossi SMM, Vitiello N, Lenzi T, Ronsse R, Koopman B, Persichetti A, et al. Sensing pressure  
599 distribution on a lower-limb exoskeleton physical human-machine interface. *Sensors*  
600 2011;11:207–27.
- 601 [54] Wan X, Liu Y, Akiyama Y, Yamada Y. Monitoring contact behavior during assisted walking with  
602 a lower limb exoskeleton. *IEEE Trans Neural Syst Rehabil Eng* 2020;28:869–77.
- 603 [55] Bennett L, Lee BY. Vertical shear existence in animal pressure threshold experiments. *Adv*  
604 *Skin Wound Care* 1988;1:18–24.
- 605 [56] Wheeler J, Mazumdar A, Marron L, Dullea K, Sanders J, Allyn K. A pressure and shear sensing  
606 liner for prosthetic sockets. *Annu Int Conf IEEE Eng Med Biol Soc IEEE Eng Med Biol Soc Annu*  
607 *Int Conf* 2016;2016:2026–9. <https://doi.org/10.1109/EMBC.2016.7591124>.
- 608 [57] Mak AFT, Zhang M, Tam EWC. Biomechanics of pressure ulcer in body tissues interacting with  
609 external forces during locomotion. *Annu Rev Biomed Eng* 2010;12:29–53.
- 610 [58] Melia M, Schmidt M, Geissler B, König J, Krahn U, Ottersbach HJ, et al. Measuring mechanical  
611 pain: the refinement and standardization of pressure pain threshold measurements. *Behav*  
612 *Res Methods* 2015;47:216–27. <https://doi.org/10.3758/s13428-014-0453-3>.
- 613 [59] Huysamen K, de Looze M, Bosch T, Ortiz J, Toxiri S, O’Sullivan LW. Assessment of an active  
614 industrial exoskeleton to aid dynamic lifting and lowering manual handling tasks. *Appl Ergon*  
615 2018;68:125–31. <https://doi.org/10.1016/j.apergo.2017.11.004>.
- 616 [60] Millard M, Sreenivasa M, Mombaur K. Predicting the Motions and Forces of Wearable  
617 Robotic Systems Using Optimal Control . *Front Robot AI* 2017;4:41.
- 618 [61] Armitage L, Buller A, Rajan G, Prusty G, Simmons A, Kark L. Clinical utility of pressure

619 feedback to socket design and fabrication. *Prosthet Orthot Int* 2019;0309364619868364.  
620 <https://doi.org/10.1177/0309364619868364>.

621 [62] Paternò L, Dhokia V, Menciassi A, Bilzon J, Seminati E. A personalised prosthetic liner with  
622 embedded sensor technology: a case study. *Biomed Eng Online* 2020;19:71.  
623 <https://doi.org/10.1186/s12938-020-00814-y>.

624 [63] Deijke V, Eng MP, Brinkfeldt K, Charnley J, Lussey D, Lussey C. Development of Prototype Low-  
625 Cost QTSS™ Wearable Flexible More Enviro-Friendly Pressure, Shear, and Friction Sensors for  
626 Dynamic Prosthetic Fit Monitoring. *Sensors* 2021;21. <https://doi.org/10.3390/s21113764>.

627 [64] Polliack AA, Sieh RC, Craig DD, Landsberger S, McNeil DR, Ayyappa E. Scientific validation of  
628 two commercial pressure sensor systems for prosthetic socket fit. *Prosthet Orthot Int*  
629 2000;24:63–73. <https://doi.org/10.1080/03093640008726523>.

630 [65] Ali S, Abu Osman NA, Eshraghi A, Gholizadeh H, Abd razak NA bin, Wan Abas WAB Bin.  
631 Interface pressure in transtibial socket during ascent and descent on stairs and its effect on  
632 patient satisfaction. *Clin Biomech* 2013;28:994–9.  
633 <https://doi.org/https://doi.org/10.1016/j.clinbiomech.2013.09.004>.

634 [66] Eshraghi A, Abu Osman NA, Gholizadeh H, Ali S, Abas WABW. Interface stress in  
635 socket/residual limb with transtibial prosthetic suspension systems during locomotion on  
636 slopes and stairs. *Am J Phys Med Rehabil* 2015;94:1–10.  
637 <https://doi.org/10.1097/PHM.000000000000134>.

638 [67] Karamousadakis M, Porichis A, Ottikkutti S, Chen D, Vartholomeos P. A Sensor-Based Decision  
639 Support System for Transfemoral Socket Rectification. *Sensors* 2021;21.  
640 <https://doi.org/10.3390/s21113743>.

641 [68] Perego P, Sironi R, Gruppioni E, Davalli A, Pittaccio S, Romanò J, et al. Design of an Innovative  
642 Integrated System for Upper Limb Prosthesis BT - Wearables in Healthcare. In: Perego P,

643 TaheriNejad N, Caon M, editors., Cham: Springer International Publishing; 2021, p. 154–60.

644 [69] Steer J, Browne M, Paton J, Rankin K, Mavrogordato M, Marter A, et al. Developing an

645 Analogue Residual Limb for DVC Analysis of Transtibial Prosthetic Socket Designs. Eur. Soc.

646 Biomech. 2019, Vienna, Austria, 2019, p. 346.

647

648