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## Abstract

The influence of the in-plane displacement and double-aperture orientation on the slope fringe formation in double-shearing-aperture speckle interferometry is discussed in detail. The research results show that the two in-plane displacement components, one parallel to and the other perpendicular to the shearing direction, have an influence on the slope fringe formation and that the double-aperture orientation also has an important influence on the slope fringe formation. A theoretical analysis and experimental results are presented. The experimental results are in good agreement with the theoretical analysis.

## Keywords

speckle, formation, fringe, interferometry, slope, influence, orientation, aperture, double, displacement, plane, shearing

## Disciplines

Engineering | Science and Technology Studies

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# Influence of in-plane displacement and double-aperture orientation on slope fringe formation in double-shearing-aperture speckle interferometry

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**Abstract.** The influence of the in-plane displacement and double-aperture orientation on the slope fringe formation in double-shearing-aperture speckle interferometry is discussed in detail. The research results show that the two in-plane displacement components, one parallel to and the other perpendicular to the shearing direction, have an influence on the slope fringe formation and that the double-aperture orientation also has an important influence on the slope fringe formation. A theoretical analysis and experimental results are presented. The experimental results are in good agreement with the theoretical analysis. © 2000 Society of Photo-Optical Instrumentation Engineers. [S0091-3286(00)01908-5]

Subject terms: double-shearing-aperture speckle interferometry; slope fringe formation; in-plane displacement; double-aperture orientation.

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## 1 Introduction

The determination of slope distribution information is of vital importance in the investigation of the out-of-plane deformation of thin plates because the slope distribution is related to the stress and strain distributions of these plates. Speckle shearing interferometry is a powerful tool in the measurement of slope distributions and has been used extensively to analyze the stress and strain fields of thin plates.<sup>1,2</sup>

In speckle shearing interferometry, the slope distribution information concerning thin plates can be obtained using either single-aperture or double-aperture speckle shearing interferometry. With double-aperture speckle shearing interferometry, the contrast of fringes is good compared with that obtained in single-aperture speckle shearing interferometry, but double-aperture speckle shearing interferometry is sensitive to the in-plane displacement components<sup>3-6</sup> and to the in-plane strain components.<sup>4-6</sup> In Ref. 3, the influence of the in-plane displacement components on the slope fringe formation in speckle grating-shearing interferometry was first studied. The research result shows that the in-plane displacement components do have an influence on the slope fringe formation in double-aperture speckle grating-shearing interferometry. In Refs. 4 to 6, the influence of the in-plane displacement components on the slope fringe formation in multiaperture speckle wedge-shearing interferometry was also investigated. We can see from the results that the in-plane displacement components have an important influence on the slope fringe formation in multiaperture wedge-shearing interferometry.

In this paper, we discuss in detail the influence of the in-plane displacement and double-shearing-aperture orientation on the slope fringe formation in double-shearing-aperture speckle interferometry, which, to our knowledge,

has not been previously investigated. A quantitative analysis and experimental results are presented.

## 2 Experimental Arrangement

The experimental arrangement is shown in Fig. 1. A collimated He-Ne laser beam normally illuminates the diffuse surface of an object. An imaging lens is focused on the diffuse surface. A mask with two apertures  $A_1$  and  $A_2$  drilled along the direction with an included angle  $\theta$  with respect to the  $x$  axis is symmetrically placed in front of the imaging lens. The scattered wavefront from the diffuse surface is divided into two wavefronts through the mask. Two shearing wedges with the same wedge angle and refractive index are axisymmetrically placed in front of apertures  $A_1$  and  $A_2$ , respectively, with the shearing direction of each shearing wedge parallel to the  $x$  axis. This experimental arrangement brings the two wavefronts coming from a point at the object plane to focus at two different points on the image plane. In other words, the wavefronts from two object points  $O_1(x + \Delta_o, y)$  and  $O_1(x - \Delta_o, y)$  through apertures  $A_1$  and  $A_2$ , respectively, are added coherently at the image plane of the imaging system, as shown in Fig. 1. The equivalent shifting magnitude of each image at the object plane is given as follows:

$$\Delta_o = d_o(\mu - 1)\alpha, \quad (1)$$

where  $d_o$  is the object distance of the imaging system,  $\mu$  is the refractive index of the shearing wedges, and  $\alpha$  is the wedge angle. With this configuration, two exposure records, one before and the other after object deformation, are made on a single photographic plate.

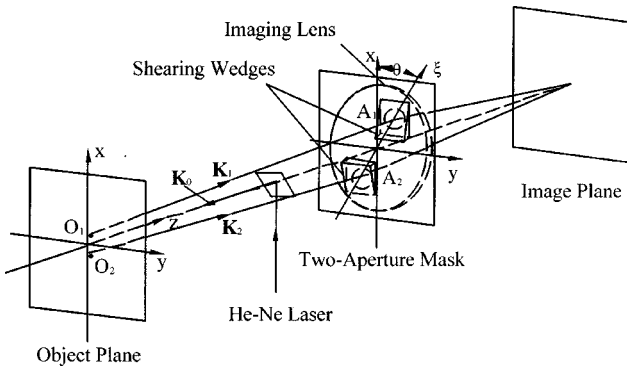


Fig. 1 Schematic of the recording system.

### 3 Theoretical Analysis

#### 3.1 Specklegram Record

Assuming that the two scattered wavefronts from the object plane through apertures  $A_1$  and  $A_2$  have amplitudes  $a_1$  and  $a_2$ , respectively, the total amplitude distribution at the image plane before deformation can be expressed as

$$U_1 = a_1 \exp[i(\varphi_1 + \beta)] + a_2 \exp[i(\varphi_2 - \beta)], \quad (2)$$

where  $\varphi_1$  and  $\varphi_2$  are the random phases corresponding respectively to the two object points  $O_1(x + \Delta_o, y)$  and  $O_1(x - \Delta_o, y)$ , and  $\beta$  is the phase corresponding to the grating-like structure in speckles introduced by the double-aperture separation. The intensity distribution at the image plane before deformation is given by

$$I_1 = |U_1|^2 = a_1^2 + a_2^2 + 2a_1a_2 \cos(\varphi_{12} + 2\beta), \quad (3)$$

where  $\varphi_{12} = \varphi_1 - \varphi_2$  is the difference of random phases.

Similarly, the total amplitude distribution at the image plane after the object is deformed can be written as

$$U_2 = a_1 \exp[i(\varphi_1 + \delta_1 + \beta)] + a_2 \exp[i(\varphi_2 + \delta_2 - \beta)], \quad (4)$$

where  $\delta_1$  and  $\delta_2$  are the phase changes of the two wavefronts caused by object deformation. According to the directions of illumination and observation, the phase changes can be expressed as follows:

$$\begin{cases} \delta_1 = (\mathbf{K}_1 - \mathbf{K}_0) \cdot \mathbf{L}(x + \Delta_o, y) = (\mathbf{K}_1 - \mathbf{K}_0) \cdot \left[ \mathbf{L}(x, y) + \frac{\partial \mathbf{L}(x, y)}{\partial x} \Delta_o \right] \\ \delta_2 = (\mathbf{K}_2 - \mathbf{K}_0) \cdot \mathbf{L}(x - \Delta_o, y) = (\mathbf{K}_2 - \mathbf{K}_0) \cdot \left[ \mathbf{L}(x, y) - \frac{\partial \mathbf{L}(x, y)}{\partial x} \Delta_o \right] \end{cases} \quad (5)$$

where  $\mathbf{K}_0$  is the propagation vector along the illumination direction,  $\mathbf{K}_1$  and  $\mathbf{K}_2$  are the propagation vectors along the observation directions, and  $\mathbf{L}(x + \Delta_o, y)$  and  $\mathbf{L}(x - \Delta_o, y)$  are the displacement vectors at the two object points  $O_1(x + \Delta_o, y)$  and  $O_1(x - \Delta_o, y)$ , respectively, as shown in Fig. 1. The intensity distribution at the image plane of the imaging system after object deformation is given by

$$I_2 = |U_2|^2 = a_1^2 + a_2^2 + 2a_1a_2 \cos(\varphi_{12} + \delta_{12} + 2\beta), \quad (6)$$

where  $\delta_{12} = \delta_1 - \delta_2$  is the difference of the phase changes.

According to Eq. (5),  $\delta_{12}$  can be expressed as

$$\delta_{12} = (\mathbf{K}_1 + \mathbf{K}_2 - 2\mathbf{K}_0) \cdot \frac{\partial \mathbf{L}(x, y)}{\partial x} \Delta_o + (\mathbf{K}_1 - \mathbf{K}_2) \cdot \mathbf{L}(x, y), \quad (7)$$

where the displacement vector  $\mathbf{L}(x, y)$  and its partial derivative vector  $\partial \mathbf{L}(x, y) / \partial x$  can be given by

$$\begin{cases} \mathbf{L}(x, y) = u(x, y)\mathbf{i} + v(x, y)\mathbf{j} + w(x, y)\mathbf{k}, \\ \frac{\partial \mathbf{L}(x, y)}{\partial x} = \frac{\partial u(x, y)}{\partial x} \mathbf{i} + \frac{\partial v(x, y)}{\partial x} \mathbf{j} + \frac{\partial w(x, y)}{\partial x} \mathbf{k}, \end{cases} \quad (8)$$

where  $\mathbf{i}$ ,  $\mathbf{j}$ , and  $\mathbf{k}$  are the unit vectors along the  $x$ ,  $y$ , and  $z$  directions, respectively. The propagation vectors  $\mathbf{K}_0$ ,  $\mathbf{K}_1$ , and  $\mathbf{K}_2$  in Eq. (7) can also be given, according to Fig. 1, by

$$\begin{cases} \mathbf{K}_0 = \frac{2\pi}{\lambda} [-\sin \gamma_0 (\mathbf{i} \cos \theta_0 + \mathbf{j} \sin \theta_0) - \mathbf{k} \cos \gamma_0], \\ \mathbf{K}_1 = \frac{2\pi}{\lambda} [\sin \gamma_1 (\mathbf{i} \cos \theta + \mathbf{j} \sin \theta) + \mathbf{k} \cos \gamma_1], \\ \mathbf{K}_2 = \frac{2\pi}{\lambda} [-\sin \gamma_2 (\mathbf{i} \cos \theta + \mathbf{j} \sin \theta) + \mathbf{k} \cos \gamma_2], \end{cases} \quad (9)$$

where  $\theta$  is the included angle between the double-aperture direction and the  $x$  axis. In the experimental arrangement in Fig. 1,  $\gamma_1, \gamma_2 \ll 1$ , which results in

$$\begin{cases} \sin \gamma_1 \approx \sin \gamma_2 \approx \frac{D}{2d_o}, \\ \cos \gamma_1 \approx \cos \gamma_2 \approx 1, \end{cases} \quad (10)$$

where  $D$  is the double-aperture separation. Therefore Eq. (9) can reduce to

$$\begin{cases} \mathbf{K}_0 = \frac{2\pi}{\lambda} [-\sin \gamma_0 (\mathbf{i} \cos \theta_0 + \mathbf{j} \sin \theta_0) - \mathbf{k} \cos \gamma_0], \\ \mathbf{K}_1 = \frac{2\pi}{\lambda} \left[ \frac{D}{2d_o} (\mathbf{i} \cos \theta + \mathbf{j} \sin \theta) + \mathbf{k} \right], \\ \mathbf{K}_2 = \frac{2\pi}{\lambda} \left[ -\frac{D}{2d_o} (\mathbf{i} \cos \theta + \mathbf{j} \sin \theta) + \mathbf{k} \right], \end{cases} \quad (11)$$

By substitution of Eqs. (8) and (11) into Eq. (7), the following equation can be obtained

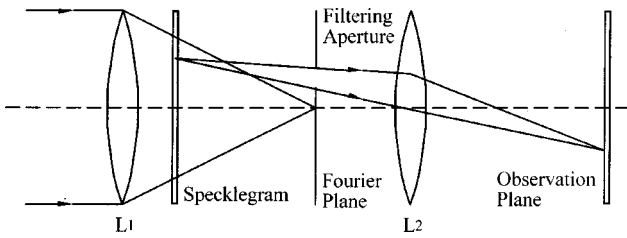


Fig. 2 Schematic of the analysis system.

$$\begin{aligned} \delta_{12} \approx & \frac{2\pi}{\lambda} 2\Delta_o [\sin \gamma_0 (\mathbf{i} \cos \theta_0 + \mathbf{j} \sin \theta_0) + \mathbf{k} (1 + \cos \gamma_0)] \\ & \cdot \frac{\partial \mathbf{L}(x,y)}{\partial x} + \frac{2\pi}{\lambda} \frac{D}{d_o} (\mathbf{i} \cos \theta + \mathbf{j} \sin \theta) \cdot \mathbf{L}(x,y) \\ = & \frac{2\pi}{\lambda} 2\Delta_o (1 + \cos \gamma_0) \frac{\partial w(x,y)}{\partial x} \\ & + \frac{2\pi}{\lambda} 2\Delta_o \sin \gamma_0 \left[ \frac{\partial u(x,y)}{\partial x} \cos \theta_0 + \frac{\partial v(x,y)}{\partial x} \sin \theta_0 \right] \\ & + \frac{2\pi}{\lambda} \frac{D}{d_o} [u(x,y) \cos \theta + v(x,y) \sin \theta]. \end{aligned} \quad (12)$$

We can see from the preceding equation that the two in-plane displacement components  $u(x,y)$  and  $v(x,y)$  have an influence on the slope fringe formation and that the double-aperture orientation  $\theta$  has also an important influence on the slope fringe formation. We can also see that the in-plane strain components  $\delta u(x,y)/\partial x$  and  $\delta v(x,y)/\partial x$  and the illumination angles  $\theta_0$  and  $\gamma_0$  influence the slope fringe formation, but when utilizing normal illumination,  $\gamma_0=0$ , the in-plane strain components and the illumination direction have no influence on the slope fringe formation, and then Eq. (12) can reduce to

$$\begin{aligned} \delta_{12} \approx & \frac{2\pi}{\lambda} 4\Delta_o \frac{\partial w(x,y)}{\partial x} + \frac{2\pi}{\lambda} \frac{D}{d_o} [u(x,y) \cos \theta \\ & + v(x,y) \sin \theta]. \end{aligned} \quad (13)$$

### 3.2 Filtering Analysis

The total intensity distribution recorded at the image plane of the imaging system as a result of double exposure records is expressed as

$$\begin{aligned} I_t = & I_1 + I_2 \\ = & 2(a_1^2 + a_2^2) + 2a_1 a_2 [\cos(\varphi_{12} + 2\beta) \\ & + \cos(\varphi_{12} + \delta_{12} + 2\beta)]. \end{aligned} \quad (14)$$

To yield information fringes, the preceding double-exposed specklegram is placed in the Fourier filtering system as shown in Fig. 2. Three diffraction halos are formed at the Fourier plane of lens  $L_1$  when subjected to Fourier filtering. The amplitude distribution at the observation plane of the analysis system by filtering via one of the two first-order halos is represented by

$$U_f = a_1 a_2 \{ \exp[i(\varphi_{12} + 2\beta)] + \exp[i(\varphi_{12} + \delta_{12} + 2\beta)] \}, \quad (15)$$

and the intensity distribution at the observation plane is given by

$$I_f = |U_f|^2 = 2a_1^2 a_2^2 (1 + \cos \delta_{12}). \quad (16)$$

We can see from Eqs. (13) and (16) that dark fringes will appear when  $\delta_{12} = (2n + 1)\pi$ , that is,

$$\begin{aligned} \frac{\partial w(x,y)}{\partial x} + \frac{D}{4\Delta_o d_o} [u(x,y) \cos \theta + v(x,y) \sin \theta] \\ = \frac{(2n + 1)\lambda}{8\Delta_o} \quad (n = 0, \pm 1, \pm 2, \dots), \end{aligned} \quad (17)$$

where  $\lambda$  is the laser wavelength. Similarly bright fringes will appear when  $\delta_{12} = 2n\pi$ , that is,

$$\begin{aligned} \frac{\partial w(x,y)}{\partial x} + \frac{D}{4\Delta_o d_o} [u(x,y) \cos \theta + v(x,y) \sin \theta] \\ = \frac{n\lambda}{4\Delta_o} \quad (n = 0, \pm 1, \pm 2, \dots). \end{aligned} \quad (18)$$

## 4 Experimental Results

The experiments were carried out using an experimental arrangement like that shown in Fig. 1. An aluminum plate with a radius of 26 mm and a thickness of 3 mm was used as the specimen at the object plane. The specimen was rigidly clamped along its edge and subjected to both an out-of-plane deformation by centrally loading at its center and an in-plane displacement by rotating around its center. The specimen surface was normally illuminated with a collimated beam from a 30-mW He-Ne laser (laser wavelength  $\lambda = 632.8$  nm) by placing a beamsplitter between the object plane and imaging lens, as shown in Fig. 1. The imaging lens had a focal distance of 240 mm and the imaging system had a magnification of 1.0. Two shearing wedges with the same wedge angle of 28 min and the same refractive index of 1.515 were axisymmetrically placed in front of a double-aperture mask with an aperture separation of 20 mm.

According to Ref. 7, the deflection distribution of a circular plate, which is loaded at its center and rigidly clamped along its boundary, is given as follows:

$$\begin{aligned} w(x,y) = w_{\max} \left( 1 - \frac{x^2 + y^2}{r^2} + \frac{x^2 + y^2}{r^2} \ln \frac{x^2 + y^2}{r^2} \right) \\ [(x^2 + y^2)^{1/2} \leq r], \end{aligned} \quad (19)$$

where  $w_{\max}$  and  $r$  are the central deflection and radius of plate, respectively. According to the preceding equation, the equation of slope distribution is expressed as follows:

$$\frac{\partial w(x,y)}{\partial x} = \frac{2w_{\max}}{r} \frac{x}{r} \ln \frac{x^2 + y^2}{r^2} \quad [(x^2 + y^2)^{1/2} \leq r]. \quad (20)$$

In addition, the in-plane displacement components respectively along the  $x$  and  $y$  directions, when subjected to an in-plane rotation around its center, can be given by

$$u(x,y) = \phi y, \quad v(x,y) = -\phi x \quad [(x^2 + y^2)^{1/2} \leq r], \quad (21)$$

where  $\phi$  is the in-plane rotation angle of the specimen. By substitution of Eqs. (20) and (21) into Eqs. (13) and (18), we can obtain the following equations:

$$\delta_{12} = \frac{2\pi}{\lambda} 4\Delta_o \frac{2w_{\max}}{r} \left( \frac{x}{r} \ln \frac{x^2 + y^2}{r^2} + \frac{D\phi r^2}{8\Delta_o d_o w_{\max}} \frac{y \cos \theta - x \sin \theta}{r} \right) \quad [(x^2 + y^2)^{1/2} \leq r], \quad (22)$$

and

$$\begin{aligned} \frac{x}{r} \ln \frac{x^2 + y^2}{r^2} + \frac{D\phi r^2}{8\Delta_o d_o w_{\max}} \frac{y \cos \theta - x \sin \theta}{r} \\ = \frac{n\lambda r}{8\Delta_o w_{\max}} \quad [(x^2 + y^2)^{1/2} \leq r, \quad n = 0, \pm 1, \pm 2, \dots]. \end{aligned} \quad (23)$$

**Experiment I.** The specimen was subjected to both an out-of-plane deflection of  $5 \mu\text{m}$  at its center and an in-plane rotation of  $2 \text{ min}$  around its center. The double-aperture orientation and shearing direction were parallel to the  $x$  axis. By substitution of the experimental parameters into Eqs. (22) and (23), we obtain

$$\delta_{12} = \frac{2\pi}{\lambda} 4\Delta_o \frac{2w_{\max}}{r} \left( \frac{x}{r} \ln \frac{x^2 + y^2}{r^2} + 0.2036 \frac{y}{r} \right) \quad [(x^2 + y^2)^{1/2} \leq r], \quad (24)$$

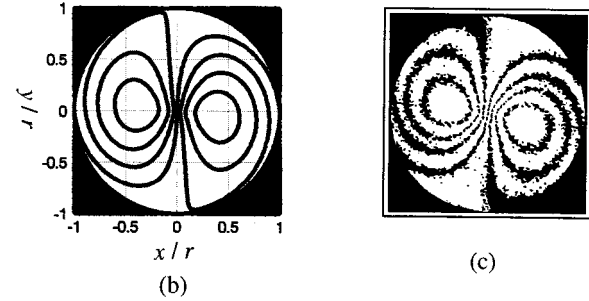
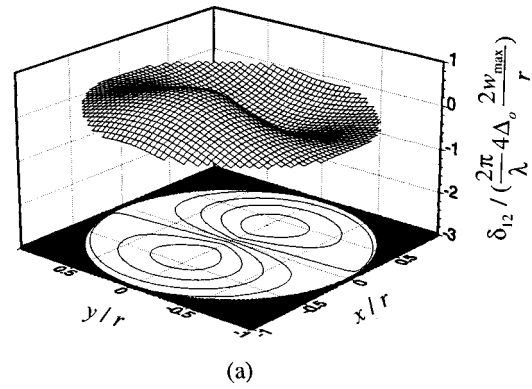
and

$$\begin{aligned} \frac{x}{r} \ln \frac{x^2 + y^2}{r^2} + 0.2036 \frac{y}{r} = 0.2044n \quad [(x^2 + y^2)^{1/2} \leq r; \\ n = 0, \pm 1, \pm 2, \dots]. \end{aligned} \quad (25)$$

**Experiment II.** The specimen was subjected to an out-of-plane deflection of  $5 \mu\text{m}$  at its center and an in-plane rotation of  $10 \text{ min}$  around its center. The double-aperture orientation was perpendicular to the  $x$  axis, while the shearing direction was still parallel to the  $x$  axis. By substitution of the experimental parameters into Eqs. (22) and (23), we obtain

$$\delta_{12} = \frac{2\pi}{\lambda} 4\Delta_o \frac{2w_{\max}}{r} \left( \frac{x}{r} \ln \frac{x^2 + y^2}{r^2} - 1.018 \frac{x}{r} \right) \quad [(x^2 + y^2)^{1/2} \leq r], \quad (26)$$

and



**Fig. 3** Theoretical and experimental results for experiment I: (a) 3-D phase distribution and its contour projection, (b) 2-D distribution of contours, and (c) experimental result.

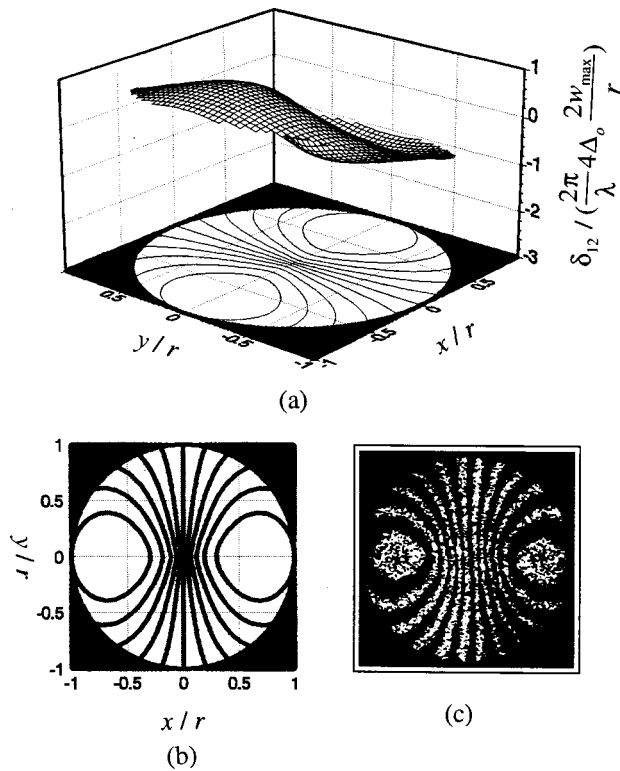
$$\begin{aligned} \frac{x}{r} \ln \frac{x^2 + y^2}{r^2} - 1.018 \frac{x}{r} = 0.2044n \quad [(x^2 + y^2)^{1/2} \leq r; \\ n = 0, \pm 1, \pm 2, \dots]. \end{aligned} \quad (27)$$

The patterns of 3-D phase distributions corresponding to experiments I and II, which are drawn according to Eqs. (24) and (26), are shown in Figs. 3(a) and 4(a), respectively. The contours of phase distributions in Figs. 3(a) and 3(b), and in Figs. 4(a) and 4(b) are, respectively, drawn according to Eqs. (25) and (27).

The experimental results for experiments I and II are shown in Figs. 3(c) and 4(c), respectively. We can see that there is hardly any difference between Figs. 3(b) and 3(c), and between Figs. 4(b) and 4(c) with respect to fringe locations and shapes.

## 5 Conclusions

The influence of the in-plane displacement and double-aperture orientation on the slope fringe formation in double-shearing-aperture speckle interferometry was discussed in detail. The research results show that all two in-plane displacement components, one parallel to and the other perpendicular to the shearing direction, have an influence on the slope fringe formation and that the double-aperture orientation has also an important influence on the slope fringe formation. It is also shown that the in-plane strain components and the illumination direction have no influence on the slope fringe formation when the object surface is normally illuminated and the imaging system axis-symmetrical. We can see from Figs. 3 and 4, respectively, that the experimental results are in good agreement with the quantitative analysis.



**Fig. 4** Theoretical and experimental results for experiment II: (a) 3-D phase distribution and its contour projection, (b) 2-D distribution of contours, and (c) experimental result.

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