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Abstract

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Abstract. To deal with the three-dimensional (3-D) point cloud loss caused by object reflection in the active fringe projection 3-D measurement, an active reflection suppression method for 3-D measurement is proposed. The method employs high-dynamic range images obtained by multiple exposure image fusion and a three-wavelength phase-shift profilometry method to achieve high-precision 3-D measurement of reflective objects. Experimental results show that, compared to traditional 3-D measurement methods, the proposed one can more effectively handle reflections thereby avoiding 3-D point cloud loss in the measurement of reflective objects. © 2019 SPIE and IS&T [DOI: 10.1117/1.JEI.28.1.013010]

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1 Introduction

Noncontact three-dimensional (3-D) measurement is widely used in quality inspection and process control because it is convenient to use and has high measurement accuracy. Active 3-D measurement technology normally has high precision and reliability, which has a variety of applications, such as heritage conservation, industrial production, and biomedical science.^{1,2} However, the mirror reflection of highly reflective objects can lead to camera saturation and thereby the loss of 3-D point cloud of the reflective parts.³ For example, Figs. 1(a) and 1(b) show an image of a plastic cylinder and the corresponding captured fringe pattern image. Due to the diffuse reflection on the surface, the camera can capture a clear fringe pattern image. In contrast, Fig. 1(c) shows the image of the shaft connector, and Fig. 1(d) shows a fringe pattern image captured by the camera with the same exposure time as Fig. 1(b), where we can see the severe mirror reflection. At present, spraying developer is often used in industry to solve this problem, but the method is time consuming and the precision is subject to the thickness of powder spraying.

In recent years, several methods are proposed to measure 3-D data in the presence of interreflections. Phase-shifting fringe projection can be combined with multiview stereo to avoid measurement error caused by diffuse reflection of object surface.⁴ Three-wavelength phase-shift profilometry (TWSP) is an effective method that can suppress the phase disturbance caused by diffuse reflections. In this method, the phase disturbance caused by diffuse reflection is same from different views, and the phase is only used to establish the relationship between the cameras. However, this method is not suitable for measuring glossy surfaces with specular reflections, because specular reflection changes with different views.

The investigation on reflection suppression has attracted much attention. In order to suppress specular reflection in fringe pattern images, Umeyama and Godin⁵ proposed to

suppress object reflection by adding polarization devices in 3-D imaging system. This method is simple to operate and effective in reflection suppression. However, it requires additional system complexity and weakens the light intensity of the collected images, thus affecting the accuracy of measurement. Waddington and Kofman⁶ proposed to handle reflection by correcting sine fringes. The intensity of the fringe pattern is adaptively adjusted, so that the maximum input gray level of the camera is kept within the normal acquisition range to avoid camera saturation. Zhang et al.⁷ used the point diffusion function and the camera corresponding function to adjust the intensity of the projection stripe to prevent the camera from overexposure. It can achieve better measurement results for different scenes. Babaie and Farahi⁸ and Babaie⁹ put forward a reflection elimination method by controlling the projection fringe intensity based on feedback. It can get high-dynamic range stripes. However, these methods may produce brightness and color distortion because spatial consistency is not fully considered in the fusion process.

In order to obtain better fringe images, Zhang et al.¹⁰ analyzed the features of phase-shifting fringe images and then produced the final fringe images from multiexposure images pixel-by-pixel by selecting the brightest but unsaturated corresponding pixels from one exposure. Liu et al.¹¹ first set the minimum and maximum precision gray can be measured by the experiment. Then the mask image sequence is calculated, and finally each pixel of the edge image is generated by selecting the brightest within the setting range of the corresponding pixel from one set of fringe images. Jiang et al.¹² fused the original fringe patterns acquired with different exposure times and illumination intensity to generate a synthetic fringe image. However, these methods rely on multiple exposures with different system configurations, which are mainly obtained through the offline calculation and cannot automatically adjust the configuration for different scenes.

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Fig. 1 The images of objects with different surface materials and the corresponding captured fringe pattern images: (a) a standard plastic cylinder, (b) a fringe pattern image of the plastic cylinder with exposure time = 80 ms, (c) an aluminum alloy shaft connector, and (d) a fringe pattern image of the metal shaft connector with exposure time = 80 ms.

To avoid the shortcomings of the above methods, a 3-D measurement reflection suppression method based on high-dynamic range image is proposed. The method adaptively selects exposure time for different scenes and adaptively fuses multiple images under different exposure times to obtain high-dynamic range phase-shifting fringe images, thus achieving to suppress reflection. In order to obtain high-quality 3-D point cloud data, an improved TWSP method is proposed, using the high-dynamic range phase-shifting fringe images, a full 3-D point cloud data of the reflective object is obtained.

The remainder of this paper is organized as follows. Section 2 elaborates the principles of the proposed multiple exposure image fusion (MEIF) method. In Sec. 3, the improved TWSP method and the process of 3-D measurement with reflection suppression are detailed. Section 4 provides experimental results and analyses, and Sec. 5 concludes this paper.

2 MEIF Method

For reflective images, the light intensity is generally $>105 \text{ cd/m}^2$, while the dynamic range of most current CMOS and CCD sensor imaging is about 60 dB. Therefore, the root cause of the reflection issue in 3-D measurement is the insufficient dynamic measurement range of cameras.^{13,14} Because of the limitation of the existing manufacturing process, it is difficult to improve cameras by hardware. In this paper, image fusion method is used to obtain a high-dynamic range image, thereby circumventing the problem of insufficient measurement range of cameras. Multiple image fusion is involved in the proposed method. In order to reduce the time of the whole reconstruction process, pixel fusion is adopted for adaptive fusion of multiple images with different exposure times.

2.1 Selection of Image Fusion Weights

For reflective objects, there are overexposure and underexposure areas in the acquired images, and images contain different effective information under different exposure times.¹² Therefore, image exposure intensity factor $B_k(x, y)$ is a key factor of image fusion. In order to assign larger fusion weights to the pixels with moderate exposure time in the image, and to assign smaller fusion weights to the pixels with excessive exposure time and insufficient exposure time, the Gauss equation is selected to assign fusion weights to each pixel in the image. Assuming that the k 'th collected gray normalized exposure image is $I_k^{\text{gray}}(x, y)$ ($k = 1, 2, \dots, N$), and N is the camera exposure time, then $B_k(x, y)$ can be calculated as

$$B_k(x, y) = \begin{cases} e^{\frac{-(I_k^{\text{gray}}(x, y) - \mu(x, y))^2}{2\sigma^2}}, & T_L < I_k^{\text{gray}}(x, y) < 1 - T_L \\ 0, & 0 \leq I_k^{\text{gray}}(x, y) \leq T_L \text{ or } 1 - T_L \leq I_k^{\text{gray}}(x, y) \leq 1 \end{cases}, \quad (1)$$

with

$$\mu(x, y) = 0.5 + 0.3 * \left[\frac{1}{N} \sum_{k=1}^N I_k^{\text{gray}}(x, y) - 0.5 \right], \quad (2)$$

where x and y are the horizontal and vertical coordinates of the image, respectively, $\mu(x, y)$ is the gray scale average of k 'th gray normalized exposure image. To avoid getting too small fusion weights from the pixel values of over-bright or over-dark images, we use a weighted method to calculate the expectation of Gauss distribution, which is shown in Eq. (2). T_L denotes the exposure threshold value of the pixel weight with Gaussian distribution, usually the range of T_L is 0.04 to 0.12 and we set it to 0.1 in this paper. σ is standard deviation of the Gaussian distribution. If $0.1 < I_k^{\text{gray}}(x, y) < 0.9$, $B_k(x, y)$ can be calculated by Gauss distribution, whose expectation $\mu(x, y)$ is between 0.35 and 0.65. To ensure that most of $I_k^{\text{gray}}(x, y)$ are in $(\mu - \sigma, \mu + \sigma)$, σ should be in (0.25, 0.55) and we set it to 0.3 in this paper.

To obtain high-quality 3-D data, the collected images should also contain rich details and edge features. In fact, images contain different details feature richness under different exposure conditions.¹⁵ Thus image details factor $C_k(x, y)$ was selected as another key factor of image fusion. Because the Laplacian has rotation invariance, Laplace filter L is selected to extract the detailed features of $I_k^{\text{gray}}(x, y)$, and the detail image $D_k(x, y)$ of $I_k^{\text{gray}}(x, y)$ are obtained. In order to reduce the image noise, the absolute value of the image after extraction of features was taken and the Gaussian low-pass filter is applied, and then the image detail factor $C_k(x, y)$ can be expressed as

$$C_k(x, y) = H(|D_k(x, y)|) = e^{\frac{-D_k^2(x, y)}{2D_0^2}}, \quad (3)$$

where

$$D_k(x, y) = L[I_k^{\text{gray}}(x, y)] = \nabla^2 I_k^{\text{gray}}(x, y), \quad (4)$$

with L being the Laplace filter. We have

$$D_k(x, y) = \sqrt{\left(x - \frac{P}{2}\right)^2 + \left(y - \frac{Q}{2}\right)^2}, \quad (5)$$

where $D(x, y)$ denotes the distance between pixel point and frequency center, D_0 is the Gaussian filter cutoff frequency, to retain as many details as possible in the images, usually the range of D_0 is 100 to 180 and we set it to 140 in this paper, P is the number of rows of $D_k(x, y)$, and Q is the number of columns of $D_k(x, y)$.

By considering exposure intensity factor and image detail factor, the fusion weight $\hat{W}_k(x, y)$ can be obtained as the product of the two key factors. In order to ensure the sum of the pixel weights is equal to 1, the figure fusion weight $\hat{W}_k(x, y)$ is normalized, which is denoted by $\hat{W}_k^{\text{norm}}(x, y)$ i.e.,

$$\hat{W}_k(x, y) = B_k(x, y) \times C_k(x, y), \quad (6)$$

$$\hat{W}_k^{\text{norm}}(x, y) = \frac{\hat{W}_k(x, y)}{\sum_{m=1}^N \hat{W}_m(x, y)}. \quad (7)$$

The normalized fusion weight $\hat{W}_k^{\text{norm}}(x, y)$ often contains noise. Recursive filter is adopted to obtain a refined image $W_k^{\text{norm}}(x, y)$ as

$$\begin{aligned} W_k^{\text{norm}}(x, y) &= \text{RF}[\hat{W}_k^{\text{norm}}(x, y), \hat{W}_{k-1}^{\text{norm}}(x, y)] \\ &= \hat{W}_k^{\text{norm}}(x, y) + K[\hat{W}_{k-1}^{\text{norm}}(x, y) - \hat{W}_k^{\text{norm}}(x, y)], \end{aligned} \quad (8)$$

where $W_{k-1}^{\text{norm}}(x, y)$ denotes the fusion weight of the previous frame image, K is the filter coefficient, for a better filtering effect, K should be greater than 0.65, and its value is taken as 0.9 in this paper.

In the end, through the fusion of N images with different exposure times, a high-dynamic range image $E(x, y)$ was obtained as

$$E(x, y) = \sum_{k=1}^N I_k^{\text{gray}}(x, y) \times W_k^{\text{norm}}(x, y). \quad (9)$$

2.2 Adaptive Selection of Image Exposure Time

A three-wavelength, six-step phase-shift method is used in this work. This method needs to collect 18 images with different wavelengths and phase shifts. If images with different exposure times are collected for fusion, $18 \times N$ images are needed in total. Choosing the value of N not only impacts the effectiveness of the fusion, but also affects the real-time performance of 3-D reconstruction process.

In addition, the selection of exposure time directly impacts the dynamic range of fused images and affects the reflection elimination in 3-D reconstruction. To handle the above problems, a method of self-adaptive exposure time selection is proposed.

Adding the images with different exposure times can effectively improve the dynamic range of image fusion, but it also increases the fusion time. Moreover, images with similar exposure time can lead to redundancy in dynamic range. So, choosing appropriate exposure times can improve the real-time performance and the accuracy of the method.

Fig. 2 The relationship between the entropy of image and exposure frequency.

Image information entropy H can effectively measure the amount of information in the image. Therefore, it is often used for measuring image fusion. If p_i is the probability of a grayscale, the image information entropy could be represented by

$$\begin{aligned} H(p_i) &= \sum_{i=1}^k p_i * \log\left(\frac{1}{p_i}\right) \\ &= p_1 * \log\left(\frac{1}{p_1}\right) + \dots + p_k * \log\left(\frac{1}{p_k}\right). \end{aligned} \quad (10)$$

Assuming that the exposure time of camera is t . When $t < t_L$ or $t > t_H$ (t_L and t_H are the minimum and maximum effective exposure time), H is < 1 . In order to find the relationship between the information entropy of images and exposures frequency, we fused N images with exposure time $T_k = t_L + \frac{t_H - t_L}{N+1} \times k$ ($k = 1, 2, 3, \dots, N$) in the same scene, as described in Sec. 2.1, and calculated the information entropy of the fused image. As shown in Fig. 2, when there were more than four exposures, the growth rate of image information entropy slows down. To reduce the operation time of the method under the premise of ensured accuracy, images with four different exposure times are selected for image fusion.

To find the relationship between the information entropy of images and exposure time, we collected four images with exposure time $T_k = t_L + \frac{t_H - t_L}{4} \times k$ ($k = 1, 2, 3, 4$) in the same complex scene. For a clearer description, we map $[t_L, t_H]$ to $[0, 120]$. As shown in Fig. 3, when camera exposure time is in $[0, 120]$, the information entropy of the image increases and then decreases with the increase of camera exposure time and reaches the peak of image information entropy at a specific exposure time. Because four images with different exposure times are needed for image fusion, the exposure time is divided into four intervals, namely, $[0, 30]$, $(30, 60]$, $(60, 90]$, and $(90, 120]$. When exposure time is too short, the image information could be missing due to underexposure. However, using dark images can effectively suppress reflection and retain the image details. On the contrary, when the exposure time is too long, overexposure could cause loss of image details, but the image basic profile information could be effectively preserved. So we should select four images in each interval and need to obtain the exposure time of the images with the maximum

Fig. 3 Adaptive selection of image exposure time, where $\delta \in (5, 10)$ and exposure frequency is 4.

information entropy in each interval. We set the left endpoint as the starting point of the search range, and δ is the search distance. As shown in Fig. 3, with $(90, 120]$ as an example, two kinds of exposure time $(30 \text{ and } 30 + \delta)$ are adopted, and two exposure images (f_{30} and $f_{30+\delta}$) are obtained. If $Hf_{30} < Hf_{30+\delta}$, $30 + \delta$ will be selected as the new search endpoint and keep searching the right side until the exposure time corresponded of the interval image information entropy is found, as the best exposure time. Finally, the optimal exposure time t_1 , t_2 , t_3 , and t_4 , and the fusion sequences image $I_k^{\text{gray}}(x, y)$ of the particular phase under certain frequency are obtained.

3 High-Dynamic Range 3-D Reconstruction Reflection Suppression Method

A high-dynamic range image can be obtained through the fusion of images under different exposure times, which solves the problem of missing local image information caused by reflection in the collection image and ensures the integrity of phase information in the reconstruction process. However, the method induces a certain amount of time cost. In order to reduce the processing time in overall reconstruction process and the problem of missing cloud points caused by false matching in the reconstruction process, an improved TWPS method is adopted in this paper. Assuming the deformation stripes collected by the imaging system is $I_k(x, y)$, the six-step phase-shift method adopted in this paper can be described as follows:

$$I_k(x, y) = A(x, y) + B(x, y) \cos \left[\phi_i(x, y) + \frac{\pi \times k}{3} \right],$$

$$k = 0, 1, 2, 3, 4, 5,$$

where $A(x, y)$ is the background light intensity, $B(x, y)$ is the modulation light intensity, and $\phi_i(x, y)$ is wrapped phase, which can be calculated as

$$\phi_i(x, y) = \arctan \left\{ \frac{I_5(x, y) - I_3(x, y)}{[I_1(x, y) + I_4(x, y)] - [I_3(x, y) + I_5(x, y)]} \right\},$$

$$i = 1, 2, 3.$$

The existing TWPS method¹⁶ uses $\lambda_1 = 21$, $\lambda_2 = 18$, and $\lambda_3 = 16$ as the modulation wavelength of projected stripes, which needs to calculate the equivalent wavelength $\lambda_{12} = 126$, $\lambda_{23} = 144$, and $\lambda_{123} = 1008$ and the corresponding synthetic wrapped phases $\phi_{12}(i, j)$, $\phi_{23}(i, j)$, and $\phi_{123}(i, j)$. Then the corresponding unwrapped phase $\Phi_3(i, j)$ corresponding to $\lambda_3 = 16$ can be calculated as

$$\Phi_3(x, y) = \phi_3(x, y) + 2\pi \left\{ \text{INT} \left[\frac{\phi_{123}(x, y)}{2\pi} \times \frac{\lambda_{123}}{\lambda_{23}} \right] \times \frac{\lambda_{23}}{\lambda_3} + \text{INT} \left[\frac{\phi_{23}(x, y)}{2\pi} \times \frac{\lambda_{23}}{\lambda_3} \right] \right\}.$$

The phase unwrapping error caused by the calculation error of $\phi_{12}(i, j)$, $\phi_{23}(i, j)$, and $\phi_{123}(i, j)$ and the multiple jump error of phase unwrapping can result in the missing of 3-D cloud points. In order to avoid the phase error caused by phase synthesis, we select $\lambda'_1 = \lambda_{123} = 1008$, $\lambda'_2 = \lambda_{23} = 144$, and $\lambda'_3 = \lambda_3 = 16$ as the modulation wavelengths of projected stripes and corresponding wrapped phase $\phi'_i(x, y)$ can be calculated by Eq. (12), where $\phi'_1(x, y) = \phi_{123}(x, y)$, $\phi'_2(x, y) = \phi_{23}(x, y)$, and $\phi'_3(x, y) = \phi_3(x, y)$.

Therefore, the unwrapped phase $\Phi'_3(x, y)$ corresponding to $\lambda'_3 = 16$ can be obtained without calculating the equivalent wavelengths λ'_{12} , λ'_{23} , and λ'_{123} of λ'_1 , λ'_2 , and λ'_3 , and the corresponding synthesized phases $\phi'_{12}(x, y)$, $\phi'_{23}(i, j)$, and $\phi'_{123}(i, j)$. When $\phi'_3(x, y) = 2\pi$, there is jump in the phase, so the unwrapped phase $\Phi'_3(x, y)$ is revised to

$$\Phi'_3(x, y) = \begin{cases} \phi'_3(x, y) + 2\pi \left\{ \text{INT} \left[\frac{\phi'_1(x, y)}{2\pi} \times \frac{\lambda'_1}{\lambda'_2} \right] \times \frac{\lambda'_2}{\lambda'_3} + \text{INT} \left[\frac{\phi'_2(x, y)}{2\pi} \times \frac{\lambda'_2}{\lambda'_3} \right] \right\}, \\ \phi'_1(x, y) \neq 2\pi \text{ and } \phi'_2(x, y) \neq 2\pi \text{ and } \phi'_3(x, y) \neq 2\pi. \\ \phi'_3(x, y) + 2\pi \left\{ \text{INT} \left[\frac{\phi'_1(x, y)}{2\pi} \times \frac{\lambda'_1}{\lambda'_2} \right] \times \frac{\lambda'_2}{\lambda'_3} + \text{INT} \left[\frac{\phi'_2(x, y)}{2\pi} \times \frac{\lambda'_2}{\lambda'_3} \right] - 1 \right\}, \\ \phi'_1(x, y) \neq 2\pi \text{ and } [\phi'_2(x, y) = 2\pi \text{ or } \phi'_3(x, y) = 2\pi]. \\ \phi'_3(x, y) + 2\pi \left\{ \text{INT} \left[\frac{\phi'_1(x, y)}{2\pi} \times \frac{\lambda'_1}{\lambda'_2} - 1 \right] \times \frac{\lambda'_2}{\lambda'_3} + \text{INT} \left[\frac{\phi'_2(x, y)}{2\pi} \times \frac{\lambda'_2}{\lambda'_3} \right] \right\}, \\ \phi'_1(x, y) = 2\pi \text{ and } \phi'_2(x, y) \neq 2\pi \text{ and } \phi'_3(x, y) \neq 2\pi. \end{cases} \quad (14)$$

In this method, $\phi'_1(x, y)$ and $\phi'_2(x, y)$ can be directly obtained by Eq. (12), without needing to calculate synthetic phase. Thus it avoids the phase error produced in image fusion, reduces the error in phase unwrapping, and improves the quality of the 3-D point cloud data. The method avoids the phase error caused by the multiple phase synthesis and

reduces the time to get the unwrapped phase, thus improving the effectiveness of the proposed method.

The high-dynamic range image obtained in the section is used for the above TWPS method, which can effectively deal with the reflection problem. An example is shown in Fig. 4.

Fig. 4 Reflection suppression method for 3-D measurement.

The use of the MEIF method requires a longer reconstruction time. It is worth mentioning that the improved TWSP method does not require the calculation of the synthetic phase. For a certain extent, it makes up the time consumed by the whole method, improves the reconstruction accuracy, and accelerates the whole reconstruction process.

4 Experimental Results and Analysis

The proposed MEIF was incorporated into our 3-D scanning system (as shown in Fig. 5), consisting of two monochrome (black and white) Gigabit cameras (Microview RS-A1300-GM60-M10) with a resolution of 1280×1024 pixels, one digital projector (LG HW300TC-JE) with a resolution of 1280×800 pixels, one Gigabit switch (D-Link DGS-1005S-CN), and a computer (DELL Optiplex 7010 MT) with a Gigabit Ethernet NIC (Intel 82579LM). Gigabit Ethernet NIC and Gigabit switch are used to control two Gigabit cameras and read the phase-shifting images captured

Fig. 6 A plane circular calibration target.

by Gigabit cameras. A workpiece of aluminum alloy with high-reflective surfaces and a workpiece of iron with high-reflective surfaces were chosen as the test samples [as shown in Figs. 1(c) and 5]. A plastic shell (as shown in Fig. 8) was measured for analyzing the reconstruction effect of 3-D point cloud using the proposed TWSP method.

To obtain 3-D reconstruction point data of objects, stereo calibration is carried out on binocular cameras using planar circular calibration target (as shown in Fig. 6). The machining accuracy of the calibration target is $15 \mu\text{m}$, and the true distance between the center of adjacent circles in horizontal direction C is 9 mm, the true distance between the center of adjacent circles in vertical direction D is also 9 mm.

We collected calibration target images from left and right cameras at five different locations, extracted the center of circles in each calibration target image, and used the camera calibration toolbox in OpenCV2.4.11 to get the camera calibration results to calibrate binocular cameras. The principle of this toolbox is based on Zhang's calibration method.¹⁷ Then the center position of all circles in the calibration target image at each shooting angle [as shown in Figs. 7(a)–7(e)] is obtained by the calibration results.

By measuring the center distance of adjacent circles in horizontal and vertical directions in each calibrated image, we get the error of camera stereo calibration as shown in Table 1.

Fig. 5 A 3-D scanning system.

Fig. 7 The center position of all circles in each calibration target image: (a) first shooting angle, (b) second shooting angle, (c) third shooting angle, (d) fourth shooting angle, (e) fifth shooting angle, and (f) all angles.

Table 1 Root-mean-square error (RMSE) and maximum errors of camera stereo calibration.

	Center distance between adjacent circles in horizontal direction (mm)	Center distance between adjacent circles in vertical direction (mm)	All center distance (mm)
RMSE	0.020	0.018	0.019
MAX error	0.047	0.059	0.059
(%) error (RMSE)	0.222	0.200	0.211

It can be seen from Table 1 that the RMSE of camera stereo calibration in this paper is 0.019 mm. The largest deviation of the camera stereo calibration is 0.211%, which meets the precise measurement requirements of complex surfaces. Then we use different TWSPSP methods to obtain the 3-D data of a plastic shell.

In Fig. 8(a), there are many missing parts of the point cloud data caused by the false matching (the areas selected by red rectangular boxes), but a complete 3-D point cloud data of a plastic packaging shell is shown in Fig. 8(b). Compared to the existing TWSPSP method, the improved TWSPSP method can effectively reduce the point cloud

Fig. 8 3-D reconstruction results of a plastic shell: (a) the 3-D reconstruction result using the existing TWSPSP method and (b) the 3-D reconstruction result using the proposed TWSPSP method.

Fig. 9 Calibration balls used in system measurement accuracy evaluation experiment: (a) dimensions of a calibration ball and (b) a picture of a calibration ball.

data loss caused by the false matching and also achieve more complete point cloud data.

We used the calibration balls shown in Fig. 9, and the measurement scheme is shown in Fig. 10 to obtain the measurement accuracy of 3-D scanning system.

In Fig. 10, the measured scene taken by the camera is divided into five regions (I to V). The calibration ball is

Fig. 10 System measurement accuracy evaluation scheme.

placed in different areas for 3-D scanning to obtain its corresponding 3-D reconstruction data in different areas. Through the measured 3-D data, calibration ball A01 and calibration ball B01 can be fitted, respectively, and obtain the diameters $\hat{d}_1$ and $\hat{d}_2$ of the two calibration balls, and the sphere centers $\hat{O}_1$ and $\hat{O}_2$ of the two calibration balls.

Then the distance between the sphere centers of two calibration balls $\hat{O}_1\hat{O}_2$ can be obtained by the coordinates of $\hat{O}_1$ and $\hat{O}_2$. We made ten measurements at each location and calculated RMSE of $\hat{d}_1$, $\hat{d}_2$, and $\hat{O}_1\hat{O}_2$ at each location, and the first five measurements and calculations are shown in Table 2.

The average of the RMSE of the $\hat{d}_1$, $\hat{d}_2$, and $\hat{O}_1\hat{O}_2$ measured at different locations is calculated to obtain the measurement accuracy of the system at different locations, and the mean of the measurement accuracy at different locations is taken as the average measurement accuracy of the system. The calculations are shown in Fig. 11.

As shown in Fig. 11, the average measurement accuracy of the system is 0.0598 mm. Compared with other locations, the measurement accuracy of location V is the highest, which is 0.0278 mm. Therefore, in actual measurement, the object to be measured should be best placed in location V.

In order to verify the effectiveness of the proposed image fusion method, the stripe images were fused under four different exposure times where the projection stripe wavelength $\lambda = 144$, and the phase shift angle is $\frac{3}{4}\pi$, which produces the corresponding high-dynamic range images shown in

Table 2 The first five measurements of calibration balls in different positions.

Key dimensions		Location I	Location II	Location III	Location IV	Location V
$\hat{d}_1$ (mm)	1	25.4692	25.3230	25.4846	25.4574	25.4319
	2	25.4562	25.4821	25.3563	25.4699	25.4487
	3	25.3469	25.4576	25.4346	25.3516	25.4176
	4	25.4740	25.4924	25.4832	25.4718	25.4203
	5	25.4928	25.4777	25.4606	25.4658	25.4353
	RMSE	0.0650	0.0733	0.0591	0.0577	0.0248
$\hat{d}_2$ (mm)	1	25.4734	25.3536	25.3372	25.4692	25.4223
	2	25.4890	25.4600	25.4910	25.4514	25.4393
	3	25.3536	25.4753	25.4821	25.3219	25.4449
	4	25.4938	25.4821	25.4890	25.4706	25.4376
	5	25.4692	25.4713	25.4778	25.4530	25.4279
	RMSE	0.0733	0.0654	0.0785	0.0633	0.0314
$\hat{O}_1\hat{O}_2$ (mm)	1	180.0423	180.1459	180.1803	180.1485	180.1312
	2	180.1765	180.0271	180.1669	180.1726	180.1189
	3	180.0196	180.0161	180.0116	180.1361	180.1208
	4	180.1823	180.1845	180.1465	180.1540	180.0788
	5	180.1326	180.1694	180.1715	180.1393	180.1357
	RMSE	0.0696	0.0735	0.0750	0.0571	0.0303

Fig. 11 Measurement accuracy of the system at different positions.

Fig. 12 Image fusion effect: (a) stripe image with 20-ms exposure time (t_1), (b) stripe image with 52-ms exposure time (t_2), (c) stripe image with 67-ms exposure time (t_3), (d) stripe image with 95-ms exposure time (t_4), and (e) the high-dynamic range image.

Figs. 12(a)–12(d). Figure 12(e) shows the high-dynamic range image obtained through the fusion of the proposed image fusion method. Table 3 compares the image information entropy of corresponding projection stripe images before and after the fusion.

As shown in Fig. 12, the images obtained through the proposed fusion method contains more detailed characteristics, and the fusion image information entropy is improved considerably compared to the images without fusion (as shown in Table 3); and the image information loss problem caused by image overexposure is effectively solved.

Fig. 13 Experiment results of an aluminum alloy shaft connector: (a) 3-D reconstruction result using the existing TWPS method, (b) 3-D reconstruction result from the existing TWPS methods combined with high-dynamic range images, (c) 3-D reconstruction result using the proposed TWPS, and (d) 3-D reconstruction result using the reflection suppression method in 3-D measurement of this paper.

To verify the effectiveness of the 3-D measurement reflection suppression method proposed in this paper, the reconstruction performances of the methods using high-dynamic range image, the existing TWPS method, and the improved three-wavelength solution phase method are compared, as shown in Figs. 13 and 14 and Table 4.

In Figs. 13 and 14, the point cloud data selected by the red rectangle boxes are the false matching areas due to the phase unwrapping error, and the point cloud data selected by the green rectangle boxes are the areas where the reflection occurred. The experimental results show that applying high-dynamic range image to existing TWPS method can also achieve more complete point cloud data, and deal with the point cloud loss caused by object reflection. Compared to the traditional three-wavelength solution method, the proposed 3-D measurement reflection suppression method can solve the point cloud loss and point cloud chaos caused by object reflection, also reduce the false matching, get high quality of point cloud data, and thereby achieve effective reflection suppression. However, as seen from Table 4, due to the adopted image fusion method, the whole reconstruction process time is increased. Considering reflection suppression effect and 3-D reconstruction time, the proposed method in

Table 3 Comparisons of image information entropy of stripe images before and after the fusion.

	Stripe image with t_1	Stripe image with t_2	Stripe image with t_3	Stripe image with t_4	The high-dynamic range image
H (bit/pixel)	3.1860	3.7157	3.9663	3.5650	4.3749

Fig. 14 Experiment results of an iron mould: (a) 3-D reconstruction result using the existing TWSP method, (b) 3-D reconstruction result from the existing TWSP methods combined with high-dynamic range images, (c) 3-D reconstruction result using the proposed TWSP, and (d) 3-D reconstruction result using the reflection suppression method in 3-D measurement of this paper.

Table 4 Comparison of various methods.

	The existing TWSP method	The existing TWSP method combined with MEIF method	The improved TWSP method	The proposed reflection suppression method
Precision	Low	High	Middle	High
Processing speed (s)	23	47	12	31
Robustness	Low	Middle	Middle	High

this paper sacrificed a little time, but it can suppress the reflection and improve the integrity and accuracy of the point clouds.

5 Conclusion

In this paper, reflection suppression methods for industrial 3-D measurement have been studied, and a reflection suppression method based on high-dynamic range image obtained by MEIF has been proposed for active 3-D measurement. According to the experimental results, compared to the traditional three-wavelength 3-D measurement method, the proposed reflection suppression method can effectively deal with the point cloud loss and chaos caused by object reflection, and further achieve high accuracy of point cloud data. In addition, compared with the existing reflection suppression methods, the proposed method uses the information entropy of the image to adjust the exposure time adaptively and finally obtains a high-dynamic range phase-shifted image for 3-D reconstruction. However, because the image fusion method in the proposed reflection suppression method

needs to traverse all the pixels in images, it may be difficult to achieve real-time 3-D data generation, which is the future improvement of this method.

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