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Abstract

In this letter, SiC nanowires were adopted to reinforce the nanoparticle-based shear thickening fluid (STF) to improve its rheological properties. The reinforced STF showed a significant increase in viscosity. A Split-Hopkinson pressure bar was implemented to evaluate the dynamic response of STF at strain rates in the range of $3 \times 10^3 - 1.2 \times 10^4$ /s. For the pure STF, the flow stress reaches a saturation value with increasing strain rates and shows almost no strain rate sensitivity, whereas the flow stress of the reinforced STF increases with strain rates, and the strain rate sensitivity to flow stress is obvious owing to the resistance of nanowires. The essence of this study is to reveal that there is a limiting value of the flow stress of traditional nanoparticle-based STF at high strain rates due to the lubrication force among particles. SiC nanowires can be used to break this limitation of the nanoparticle-based STF.

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Dynamic response of shear thickening fluid reinforced with SiC nanowires under high strain rates

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In this letter, SiC nanowires were adopted to reinforce the nanoparticle-based shear thickening fluid (STF) to improve its rheological properties. The reinforced STF showed a significant increase in viscosity. A Split-Hopkinson pressure bar was implemented to evaluate the dynamic response of STF at strain rates in the range of 3×10^3 – 1.2×10^4 /s. For the pure STF, the flow stress reaches a saturation value with increasing strain rates and shows almost no strain rate sensitivity, whereas the flow stress of the reinforced STF increases with strain rates, and the strain rate sensitivity to flow stress is obvious owing to the resistance of nanowires. The essence of this study is to reveal that there is a limiting value of the flow stress of traditional nanoparticle-based STF at high strain rates due to the lubrication force among particles. SiC nanowires can be used to break this limitation of the nanoparticle-based STF. *Published by AIP Publishing.* [<http://dx.doi.org/10.1063/1.4994066>]

The study on energy absorption and penetration resistance of materials/structures has attracted considerable interest in the field of armor systems. Many efforts have been done on materials such as metal foam,¹ ceramic,² and Kevlar fabrics.³ Recently, some works focused on the integration of shear thickening fluid (STF) in soft armor systems to improve ballistic performance.^{4–7} When the fabrics impregnated with STF are subjected to impact loading, the viscosity of STF in fabrics increases sharply at a certain shear rate. Part of the energy is dissipated through the increased viscosity of STF;^{8,9} further, the sliding of the fibers is prevented by the STF in the fabrics, which increases the loading capacity of the fabrics. Thus, viscosity is an essential property of STF required in various applications.^{10,11} However, the viscosity of STF relies on the lubrication force, which is influenced by the material, size, and volume fraction of the nanoparticles.^{12–14} Currently, STF is mainly prepared from fumed silica or sub-micron particles, because of which it is difficult to improve the viscosity of STF based on nano-particles.¹⁵ To address this issue, we used SiC nanowires to reinforce the nanoparticle-based STF, which was expected to increase the viscosity by hindering the flow of nanoparticles.

In addition, we also tested the viscosity and dynamic flow stress of the reinforced STF to demonstrate the effectiveness of this method at high strain rates. STF undergoes high strain rate loading in the order of 10^3 to 10^5 /s in applications involving energy absorption and vibration control, such as fabrics impregnated with STF against ballistic loading^{16,17} and vibration control by squeeze flow of STF,¹⁸ whereas at present, the dynamic behavior of STF is mainly characterized by a rheometer at strain rates of the order of 10^3 /s.^{19,20} Moreover, some studies have been conducted on

the numerical simulation of fabric or squeeze flow with STF,²¹ where the dynamic material parameters at high strain rates are in urgent demands.

In this letter, SiC nanowires were used to reinforce pure silica nanoparticle-based STF, and then the dynamic response of the pure and reinforced STFs at high strain rates was investigated using the Split-Hopkinson pressure bar (SHPB). Pure STF consists of silica nanoparticles and polyethylene glycol, and the silica nanoparticles with a diameter approximately 400 nm were fabricated using the Stober method. Then, the specific amount of SiC nanowires [product of Nanjing XF Nano Company, as shown in Fig. 1(a)] was dispersed by the ultrasonic method and added into pure STF to improve the rheological properties. The total volume fraction of the solid phase in the STF was 56 vol. %, as shown in Table I.

The viscosities of STFs with/without SiC nanowires were tested at shear rates in the range of 10^{-3} –100/s with a rheometer (Anton-Paar MCR301) at a temperature of 25 °C. As shown in Fig. 1(b), there are three phases in each curve: shear thinning, shear thickening, and again shear thinning. The viscosity of the reinforced STF is significantly higher compared to that of pure STF. At low shear rates, the viscosity values of the STF reinforced with 0.625 vol. % and 1.25 vol. % SiC nanowires are about 300 Pa s and 750 Pa s, respectively, which are several times larger than those of pure STF. In the shear thickening phase, the maximum viscosities of STF with and without SiC nanowires are approximately 587 Pa s and 465 Pa s, respectively, and the increase in amplitude is approximate to 26%. Although the viscosity of the STF with 1.25 vol. % SiC nanowires is the highest at the low strain rate, the viscosity in the shear thickening zone is approximately 300 Pa s, which is almost the same as pure STF but less than the STF with 0.625 vol. % SiC nanowires. We considered that the excessive quantity of nanowires

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FIG. 1. SiC nanowires in STF and its viscosity. (a) SEM graphs of SiC nanowires; and (b) Curves of viscosity-shear rates of samples A, B, and C.

TABLE I. Volume fraction of the solid phase in different STFs.

Sample No.	A	B	C
Volume fraction of SiC nanowires (vol. %)	0	0.625	1.250
Volume fraction of SiO ₂ (vol. %)	56	55.375	54.750

presented the nanoparticles in the case of 1.25 vol. %, which made the chain of nanoparticles unstable.

The SHPB is widely used to characterize dynamic mechanical properties of materials, which consists of a strike bar, an incident bar, and a transmission bar.^{7,22,23} During the test, the incident wave, reflection wave, and transmission wave are recorded using strain gauges mounted on the incident and transmission bars. The dynamic stress and strain can be calculated using the following formula:

$$\sigma = \frac{A_B}{A_S} E \varepsilon_T \quad \varepsilon = \frac{2c}{l} \int \varepsilon_R dt \quad \dot{\varepsilon} = \frac{2c}{l} \varepsilon_R, \quad (1)$$

where σ and ε are the dynamic stress and strain, respectively; c is the stress wave velocity in the pressure bar; ε_R and ε_T are the reflection and transmission stress waves, respectively; A_B and A_S and l are the cross-sectional area of the bar and specimen and the length of the specimen, respectively. All the pressure bars are made of aluminum due to the low impedance of STF. The pressure bar is 40 mm in diameter, the incident and transmission bars are both 1800 mm in length (elastic modulus $E_{AL} = 70$ GPa, density $\rho = 2.71$ g/cm³, and wave velocity $c = 5218$ m/s), and the strike bar is 300 mm long. The schematic graph of SHPB is shown in Fig. 2. The sampling rate is 5 MHz. The specimen is 1 mm in thickness and 40 mm in diameter.^{22–24}

A typical stress wave obtained in the experiments is shown in Fig. 3(a). The dynamic stress-strain curves are shown in Figs. 3(b)–3(d). The strain rate has a significant influence on the flow stress in all the STF samples. The flow stress of pure STF increases as the strain rate increases, but such an increasing tendency decreases when the strain rate

exceeds 5000/s. In addition, the flow stress of pure STF reaches a saturated value of approximately 48.03 MPa at higher shear rates. However, the STFs reinforced with SiC nanowires do not show such tendency and saturated value, and the flow stress continues to increase with the strain rate. Moreover, the maximum flow stress of the STF reinforced with SiC nanowires is approximately 70 MPa, which shows that SiC nanowires have a significant influence on the flow stress at different strain rates, as shown in Fig. 3(d).

In the SHPB tests, STF samples were compressed between two pressure bars, which can be considered as squeeze flow, as shown in Fig. 3(e). According to the squeeze flow theory,¹⁵ both normal and shear stresses in the STF are induced by dynamic compression. In the case of pure STF, the lubrication force among the nanoparticles suffers the flow stress produced at low strain rates, namely, the flow stress can increase with the strain rate within the range of the lubrication force. Once the flow stress is larger than the lubrication force at a certain strain rate, STF would flow in the radial direction, which results in no obvious increment in flow stress at high strain rates, namely, the flow stress reaches a saturated value. In the case of reinforced STF, although the squeeze force acts on the STF, SiC nanowires prevent the flow of nanoparticles in the radial direction, which results in an increase in flow stress. Therefore, the greater the squeeze force, the larger the increase in flow stress, which corresponds to the strain rate sensitivity to flow stress in reinforced STF at high strain rates.

The peak stresses at different strain rates are shown in Fig. 4(a). At strain rates in the range of 3000/s–12 000/s, the peak stresses in pure STF are approximately 37.2 MPa, 45.6 MPa, 47.9 MPa, and 48.1 MPa, whereas those of the STF reinforced with 1.25 vol. % SiC nanowires are 41.86 MPa, 52.86 MPa, 63.87 MPa, and 74.41 MPa. It is clear that the reinforced STFs show significant strain rate sensitivity compared to pure STF.

The energy absorption E is defined as²⁵

$$E = E_{I-S} - E_{T-S} = \frac{c_B A_B}{E_B} \int_0^T \sigma_{I-S}^2(t) dt - \frac{c_B A_B}{E_B} \int_0^T \sigma_{T-S}^2(t) dt, \quad (2)$$

where E_{I-S} and σ_{I-S} are the incident energy and incident pulse, respectively, at the front specimen-bar interface; E_{T-S} and σ_{T-S} are the transmission energy and transmission pulse, respectively, at the back specimen-bar interface. The energy absorption levels at different strain rates are shown in Fig. 4(b). It is evident that the reinforced STF has a higher

FIG. 2. Schematic graph of SHPB in the experiment.

FIG. 3. SHPB experimental results at high strain rates. (a) Typical stress wave; (b)–(d) Dynamic stress-strain curves; (b) pure STF; (c) STF with 0.625 vol. % SiC nanowires; (d) STF with 1.250 vol. % SiC nanowires; and (e) schematic graph of the deformation mechanism of STF with/without SiC nanowires.

FIG. 4. Peak stress and energy absorption of STF. (a) Peak stress at different strain rates; and (b) Energy absorption at different strain rates.

energy absorption capacity compared to the pure STF. The tendency is in agreement with the strain rate sensitivity of the STF.

In summary, SiC nanowires were used to reinforce the STF, which resulted in a significant increase in viscosity compared to pure STF. In the SHPB experiments, the flow stress of pure STF reached a saturated value, whereas reinforced STF showed a significant increase in flow stress with strain rate. We considered that SiC nanowires prevented the flow of silica nanoparticles in the reinforced STF, which increased the normal and shear stresses at high strain rates. It means that the reinforced STF can bear a larger dynamic

loading than pure STF, and this improvement will be useful in future applications.

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