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Publication Details

Patel, V. Ishvarbhai., Liang, Q. Quan. & Hadi, M. N. S. (2012). Inelastic stability analysis of high strength rectangular concrete-filled steel tubular slender beam-columns. *Interaction and Multiscale Mechanics*, 5 (2), 91-104.

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Inelastic stability analysis of high strength rectangular concrete-filled steel tubular slender beam-columns

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(Received July 15, 2011, Revised November 8, 2011, Accepted April 4, 2012)

Abstract. There is relatively little numerical study on the behavior of eccentrically loaded high strength rectangular concrete-filled steel tubular (CFST) slender beam-columns with large depth-to-thickness ratios, which may undergo local and global buckling. This paper presents a multiscale numerical model for simulating the interaction local and global buckling behavior of high strength thin-walled rectangular CFST slender beam-columns under eccentric loading. The effects of progressive local buckling are taken into account in the mesoscale model based on fiber element formulations. Computational algorithms based on the Müller's method are developed to obtain complete load-deflection responses of CFST slender beam-columns at the macroscale level. Performance indices are proposed to quantify the performance of CFST slender beam-columns. The accuracy of the multiscale numerical model is examined by comparisons of computer solutions with existing experimental results. The numerical model is utilized to investigate the effects of concrete compressive strength, depth-to-thickness ratio, loading eccentricity ratio and column slenderness ratio on the performance indices. The multiscale numerical model is shown to be accurate and efficient for predicting the interaction buckling behavior of high strength thin-walled CFST slender beam-columns.

Keywords: concrete-filled steel tubes; high strength materials; inelastic analysis; local buckling.

1. Introduction

Although high strength thin-walled rectangular concrete-filled steel tubular (CFST) slender beam-columns are frequently used in high rise composite buildings, the understanding of their fundamental behavior is still not sufficient and efficient analysis and design methods have not been developed owing to the lack of experimental and numerical research on this type of composite columns. The use of the high strength thin-walled steel tubes leads to economical designs but causes local buckling, which reduces the ultimate loads of CFST columns. The effects of progressive local buckling have not been considered in existing nonlinear inelastic methods of analysis for CFST slender beam-columns. These methods may overestimate the ultimate loads of CFST beam-columns. This paper aims to develop a multiscale numerical model for simulating the interaction behavior of

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local and global buckling of high strength thin-walled CFST slender beam-columns under combined axial load and bending.

Experimental studies on the behavior of CFST short columns have been conducted by many researchers (Schneider 1998, Han 2002, Hu *et al.* 2003, Sakino *et al.* 2004, Ellobody *et al.* 2006). However, experimental studies on high strength thin-walled CFST slender beam-columns under axial load and bending have been very limited. Bridge (1976) undertook tests to examine the effects of eccentricity, column slenderness ratio and biaxial bending on the behavior of normal strength square CFST slender beam-columns. Shakir-Khalil and Zeghiche (1989) presented experimental results of normal strength CFST slender beam-columns under axial load and bending. Zhang *et al.* (2003) and Liu (2004, 2006) performed tests on the behavior of high strength rectangular CFST beam-columns under eccentric loading.

Compared to experimental methods, numerical analysis techniques are cost-effective tools that can be used to predict the behavior of high strength CFST slender beam-columns. Lakshmi and Shanmugam (2002) proposed a semi-analytical model for the inelastic analysis of CFST slender beam-columns under biaxial bending. However, their model did not consider the effects of local buckling, concrete confinement and concrete tensile strength. Liang (2009a,b) developed a performance-based analysis (PBA) technique for simulating the behavior of thin-walled CFST short beam-columns under axial load and biaxial bending. The PBA technique accounts for the effects of progressive local buckling. Moreover, Liang (2011a,b) developed numerical models for the nonlinear analysis of high-strength circular CFST slender beam-columns under eccentric loading.

Multiscale models have been developed for predicting the behavior of reinforced and prestressed concrete walls (Laskar *et al.* 2009) and of reinforced concrete beams (Nagarajan *et al.* 2010). In this paper, a multiscale numerical model is presented for simulating the interaction buckling behavior of high strength thin-walled rectangular CFST slender beam-columns under eccentric loading. The mesoscale model is described, which is based on the accurate fiber element method and incorporates the material models and the effects of local and post-local buckling of steel tube walls under stress gradients. Computational procedure is presented that implements the macroscale model for predicting the load-deflection responses of CFST slender beam-columns. Performance indices are used to quantify the performance of high strength concrete and steel tube and strength reduction due to column slenderness ratio. The verification and applications of the multiscale model are provided.

2. Mesoscale simulation

2.1 Fiber element model

The mesoscale model is developed to simulate the inelastic behavior of composite cross-sections and is based on the accurate fiber element method (Liang 2009a). The rectangular CFST beam-column section is discretized into fiber elements as depicted in Fig. 1. Each fiber element can be assigned either steel or concrete material properties. The model assumes that plane section remains plane after deformation, which leads to a linear strain distribution through the depth of the section. The fiber strains can be calculated from the curvature (ϕ) and the neutral axis depth (d_n). Fiber stresses are calculated from fiber strains using the material uniaxial stress-strain relationships.

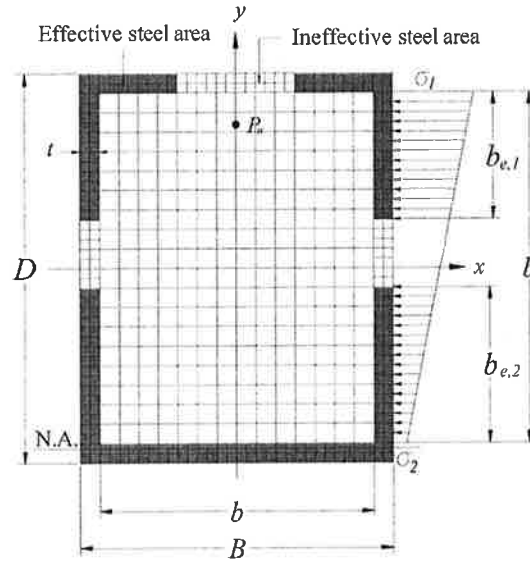


Fig. 1 Fiber element discretization of CFST column section

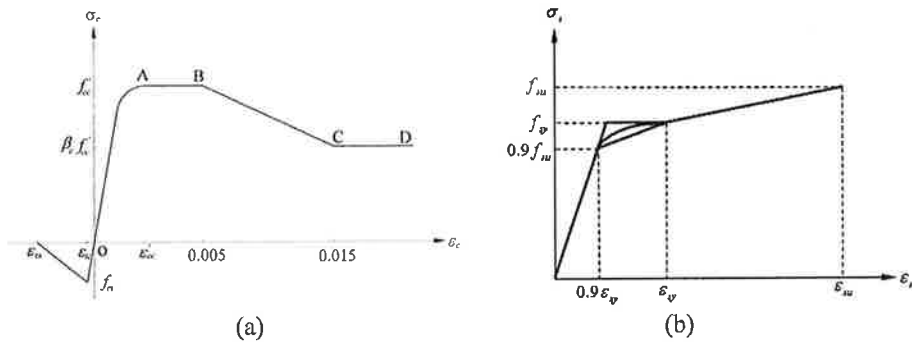


Fig. 2 Material constitutive models: (a) concrete and (b) structural steels

2.2 Material constitutive model for concrete

The confinement provided by the steel tube increases the ductility of the concrete core in a CFST column but not its compressive strength. A general stress-strain curve for concrete in CFST columns shown in Fig. 2(a) is used in the mesoscale model (Liang 2009a). The part OA of stress-strain curve is modeled using the equations suggested by Mander *et al.* (1988) as

$$\sigma_c = \frac{f'_{cc} \lambda (\epsilon_c / \epsilon'_{cc})}{\lambda - 1 + (\epsilon_c / \epsilon'_{cc})^\lambda} \quad (1)$$

$$\lambda = \frac{E_c}{E_c - (f'_{cc} / \epsilon'_{cc})} \quad (2)$$

$$E_c = 3320\sqrt{f'_{cc}} + 6900 \text{ (MPa)} \quad (3)$$

where σ_c is the compressive concrete stress, f'_{cc} is the effective compressive strength of concrete, ε_c is the compressive concrete strain and ε'_{cc} is the strain at f'_{cc} and E_c is the Young's modulus of concrete. The strain ε'_{cc} is between 0.002 and 0.003 depending on the effective compressive strength of concrete (Liang 2009a). The effective compressive strength of concrete (f'_{cc}) is taken as $\gamma_c f'_c$, where γ_c is the strength reduction factor proposed by Liang (2009a) to account for the column size effect and is expressed by

$$\gamma_c = 1.85D_c^{-0.135} \quad (0.85 \leq \gamma_c < 1.0) \quad (4)$$

where D_c is taken as the larger of $(B - 2t)$ and $(D - 2t)$ for a rectangular cross-section, B is the width of the cross-section, D is the depth of the cross-section and t is the thickness of the steel tube wall as shown in Fig. 2(a).

The model for parts AB , BC and CD of the stress-strain curve for concrete as shown in Fig. 2(a) was given by Liang (2009a) as

$$\sigma_c = \begin{cases} f'_{cc} & \text{for } \varepsilon'_{cc} < \varepsilon_c < 0.005 \\ \beta_c f'_{cc} + 100(0.015 - \varepsilon_c)(f'_{cc} - \beta_c f'_{cc}) & \text{for } 0.005 < \varepsilon_c \leq 0.015 \\ \beta_c f'_{cc} & \text{for } \varepsilon_c > 0.015 \end{cases} \quad (5)$$

where β_c was proposed by Liang (2009a) based on experimental results presented by Tomii and Sakino (1979) and is given by

$$\beta_c = \begin{cases} 1.0 & \text{for } B_s/t \leq 24 \\ 1.5 - B_s/48t & \text{for } 24 < B_s/t \leq 48 \\ 0.5 & \text{for } B_s/t > 48 \end{cases} \quad (6)$$

where B_s is taken as the larger of B and D for a rectangular cross-section.

The stress-strain curve for concrete in tension is shown in Fig. 2(a). The concrete tensile strength is taken as $0.6\sqrt{f'_{cc}}$ and ultimate strain is taken as 10 times of the strain at cracking.

2.3 Material constitutive model for structural steels

Steel tubes are usually made of high strength structural steel, cold-formed steel or mild structural steel. For mild structural steels, an idealized tri-linear stress-strain curve is assumed as shown in Fig. 2(b), where f_{sy} and f_{su} are the yield stress and tensile strength of the steel respectively. An idealized linear-rounded-linear stress-strain curve is used for cold-formed steels. The rounded part in the curve can be modeled by a formula proposed by Liang (2009a). For high strength steels, the rounded part is replaced by a straight line.

2.4 Local and post-local buckling

The effects of local and post-local buckling of high strength CFST beam-columns are taken into account in the mesoscale model. For a CFST column under axial load and bending, the steel tube walls may be subjected to compressive stress gradients as depicted in Fig. 1. The classical elastic local buckling theory cannot be used to determine the initial local buckling stress of thin steel plates with initial geometric imperfections (Liang *et al.* 2007). The formulas proposed by Liang *et al.* (2007) are therefore incorporated in the mesoscale model to determine the initial local buckling stresses of steel tube walls under stress gradients.

The effective width concept is usually used to determine the post-local buckling strength of thin steel plates under uniform compression or stress gradients as shown in Fig. 1. The effective widths b_{e1} and b_{e2} shown in Fig. 1 are given by Liang *et al.* (2007)

$$\frac{b_{e1}}{b} = \begin{cases} 0.2777 + 0.01019(b/t) - 1.972 \times 10^{-4}(b/t)^2 + 9.605 \times 10^{-7}(b/t)^3 & \text{for } \alpha_s > 0.0 \\ 0.4186 - 0.002047(b/t) + 5.355 \times 10^{-5}(b/t)^2 - 4.685 \times 10^{-7}(b/t)^3 & \text{for } \alpha_s = 0.0 \end{cases} \quad (7)$$

$$\frac{b_{e2}}{b} = (2 - \alpha_s) \frac{b_{e1}}{b} \quad (8)$$

where b is the clear width of a steel web or flange of the box section, and $\alpha_s = \sigma_2/\sigma_1$, where σ_1 and σ_2 are the maximum and minimum edge stresses acting on the steel tube wall.

In the mesoscale model, the progressive post-local buckling is modeled by gradually redistributing the normal stresses within the steel tube wall under increasing compression load based on the stress levels (Liang 2009a). After initial local buckling, steel fiber stresses are updated to account for post-local buckling effects.

2.5 Stress resultants

Axial force and moments carried by a CFST column section are determined as stress resultants by integration as follows

$$P = \sum_{i=1}^{ns} \sigma_{s,i} A_{s,i} + \sum_{j=1}^{nc} \sigma_{c,j} A_{c,j} \quad (9)$$

$$M_x = \sum_{i=1}^{ns} \sigma_{s,i} A_{s,i} y_i + \sum_{j=1}^{nc} \sigma_{c,j} A_{c,j} y_j \quad (10)$$

$$M_y = \sum_{i=1}^{ns} \sigma_{s,i} A_{s,i} x_i + \sum_{j=1}^{nc} \sigma_{c,j} A_{c,j} x_j \quad (11)$$

where P is the axial force, $\sigma_{s,i}$ is the stress of steel fiber i , $A_{s,i}$ is the area of steel fiber i , $\sigma_{c,j}$ is the stress of concrete fiber j , $A_{c,j}$ is the area of concrete fiber j , x_i and y_i are the coordinates of

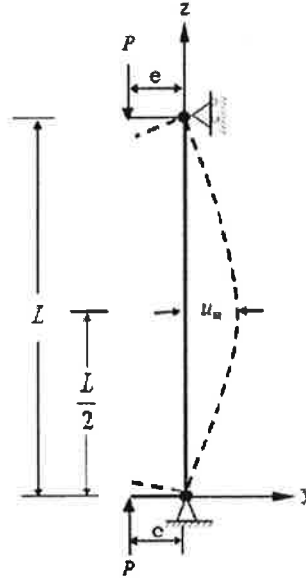


Fig. 3 Pin-ended beam-column model

steel element i , x_j and y_j are the coordinates of concrete element j , ns is the total number of steel fiber elements and nc is the total number of concrete fiber elements.

3. Macroscale simulation

3.1 Macroscale model

The macroscale model for a pin-ended beam-column under axial load at an eccentricity e is shown in Fig. 3. The deflected shape of the beam-column is assumed to be part of sine wave and is expressed by

$$u = u_m \sin\left(\frac{\pi z}{L}\right) \quad (12)$$

where L is the effective length of the beam-column and u_m is the deflection at the mid-height.

The curvature at the mid-height of the beam-column can be obtained as

$$\phi_m = \left(\frac{\pi}{L}\right)^2 u_m \quad (13)$$

The external moment at the mid-height of the beam-column with an initial geometric imperfection u_o at the mid-height can be calculated by

$$M_{me} = P(e + u_m + u_o) \quad (14)$$

To compute the load-deflection curve for a CFST slender beam-column under eccentric loading, the deflection at the column mid-height (u_m) is gradually increased. The curvature ϕ_m at the

column mid-height is computed from the deflection u_m . The neutral axis depth is then adjusted to achieve the moment equilibrium at the mid-height of the beam-column. The following equilibrium equation must be satisfied

$$P(e + u_m + u_o) - M_{mi} = 0 \quad (15)$$

where M_{mi} is the internal moment carried by the section.

3.2 Numerical solution method

Iterative numerical algorithms based on the Müller's method (Müller 1956) are developed to obtain nonlinear solutions (Patel *et al.* 2012a, b). The Müller's method requires three starting values of the neutral axis depth $d_{n,1}$, $d_{n,2}$ and $d_{n,3}$. The corresponding residual moments $r_{pu,1}$, $r_{pu,2}$ and $r_{pu,3}$ are calculated from these initial values. The new neutral axis depth $d_{n,4}$ that approaches the true value is determined by the following equations

$$d_{n,4} = d_{n,3} + \frac{-2c_m}{b_m \pm \sqrt{b_m^2 - 4a_m c_m}} \quad (16)$$

$$a_m = \frac{(d_{n,2} - d_{n,3})(r_{pu,1} - r_{pu,3}) - (d_{n,1} - d_{n,3})(r_{pu,2} - r_{pu,3})}{(d_{n,1} - d_{n,2})(d_{n,1} - d_{n,3})(d_{n,2} - d_{n,3})} \quad (17)$$

$$b_m = \frac{(d_{n,1} - d_{n,3})^2(r_{pu,2} - r_{pu,3}) - (d_{n,2} - d_{n,3})^2(r_{pu,1} - r_{pu,3})}{(d_{n,1} - d_{n,2})(d_{n,1} - d_{n,3})(d_{n,2} - d_{n,3})} \quad (18)$$

$$c_m = r_{pu,3} \quad (19)$$

where r_{pu} is the residual moment at the mid-height of the column, which is given by

$$r_{pu} = P(e + u_m + u_o) - M_{mi} \quad (20)$$

To obtain converged solutions, the values of $d_{n,1}$, $d_{n,2}$ and $d_{n,3}$ and residual moments $r_{pu,1}$, $r_{pu,2}$ and $r_{pu,3}$ need to be exchanged and Eq. (16) is used to adjust the d_n (Patel *et al.* 2012a).

3.3 Computational procedure

Computational algorithms have been developed to implement the macroscale model for thin-walled CFST slender beam-columns incorporating the mesoscale model. The main steps of the computational procedure are given as follows:

- (1) Discretize composite section into fine fiber elements.
- (2) Initialize the mid-height deflection: $u_m = \Delta u_m$.
- (3) Compute the curvature ϕ_m at the mid-height of the slender beam-column.
- (4) Initialize $d_{n,1} = D/4$, $d_{n,2} = D/2$ and $d_{n,3} = D$.
- (5) Calculate fiber stresses using material models.
- (6) Check local buckling and redistribute steel fiber stresses accordingly.
- (7) Compute internal moment M_{mi} and external moment M_{me} .
- (8) Calculate residual moments $r_{pu,1}$, $r_{pu,2}$ and $r_{pu,3}$ corresponding to $d_{n,1}$, $d_{n,2}$ and $d_{n,3}$.
- (9) Adjust the neutral axis depth d_n using the Müller's method.

- (10) Calculate fiber stresses using material models.
- (11) Check local buckling and redistribute steel fiber stresses accordingly.
- (12) Compute internal moment M_{mi} and external moment M_{me} .
- (13) Repeat Steps (9)-(12) until $|r_{pu}| < 10^{-4}$.
- (14) Increase the mid-height deflection of the beam-column by $u_m = u_m + \Delta u_m$.
- (15) Repeat Steps (3)-(14) until the ultimate load P_u is obtained or the deflection limit is reached.
- (16) Plot the axial load-deflection curve.

4. Performance indices

Performance indices that evaluate the contributions of steel and concrete components to the ultimate strengths of CFST slender beam-columns can be used to study economical composite designs. The steel contribution ratio is used to quantify the contribution of the hollow steel tubular column to the ultimate strength of the CFST slender beam-column and is defined as

$$\xi_s = \frac{P_{u,steel}}{P_u} \quad (21)$$

where $P_{u,steel}$ is the ultimate axial strength of the calculated hollow steel slender beam-column and P_u is the ultimate axial strength of the CFST slender beam-column. The ultimate axial strength $P_{u,steel}$ is calculated by setting the concrete compressive strength to zero in the numerical analysis while other conditions remain the same as the CFST beam-column.

The concrete contribution ratio is used to determine the contribution of the concrete core to ultimate strength of the CFST slender beam-column, which is defined as

$$\xi_c = \frac{P_u - P_{u,steel}}{P_u} \quad (22)$$

The strength reduction factor is used to measure the performance of a CFST slender beam-column over its section and is defined as

$$\alpha_c = \frac{P_u}{P_o} \quad (23)$$

where P_o is the ultimate axial strength of the beam-column section under axial compression.

5. Verification

The ultimate axial strengths of uniaxially loaded CFST slender beam-columns predicted by the numerical model are compared with experimental results in Table 1, where E_s is the Young's modulus. Specimens SCH-1, SCH-2 and SCH-7 were tested by Bridge (1976) while test results of specimens E03, E04, E07, E08, E11, E12, L1, L2, L3 and L4 were provided by Liu (2004, 2006) and specimens M1, M4, M6, M7 and M8 were tested by Zhang *et al.* (2003). In Table 1, the concrete cylinder compressive strength (f'_c) was taken as 0.85 times the concrete cube compressive strength (f_{cu}). It can be observed from Table 1 that the predicted ultimate axial strengths are in good agreement with corresponding test results. The mean value of the predicted axial strength

Table 1 Comparison of predicted and experimental ultimate axial strengths of CFST columns

Specimens	$B \times D \times t$ (mm)	D/t	L (mm)	e (mm)	u_0 (mm)	f'_c (MPa)	f_{sy} (MPa)	f_{su} (MPa)	E_s (GPa)	$P_{u.exp}$ (KN)	$P_{u.num}$ (KN)	$\frac{P_{u.num}}{P_{u.exp}}$
SCH-1	203.7 × 203.9 × 9.96	20	2130	38	1.19	29.9	291	410	205	1956	1995.73	1.02
SCH-2	204.0 × 203.3 × 10.01	20	3050	0	1.4	31.1	290	410	205	2869	2907.4	1.01
SCH-7	152.5 × 152.3 × 6.48	24	3050	38	0.51	31.1	254	410	205	680	734.0	1.08
E03	150 × 150 × 4.18	36	2170	30		60	550	608	207	1330	1252.42	0.93
E04	150 × 150 × 4.18	36	2170	60		70	550	608	207	1020	972.74	0.95
E07	80 × 120 × 4.18	29	1740	20		60	550	608	207	660	740.56	1.12
E08	80 × 120 × 4.18	29	1740	20		70	550	608	207	855	776.14	0.91
E11	80 × 160 × 4.18	38	2310	60		60	550	608	207	670	640.76	0.96
E12	80 × 160 × 4.18	38	2310	30		70	550	608	207	1020	909.89	0.89
L1	100 × 150 × 4	38	2600	15		60	495	581	206	1130	1013.86	0.90
L2	100 × 150 × 4	38	2600	30		60	495	581	206	884	804.82	0.91
L3	100 × 150 × 4	38	2600	45		60	495	581	206	711	674.74	0.95
L4	100 × 150 × 4	38	2600	60		60	495	581	206	617	587.37	0.95
M1	149.44 × 149.44 × 2.89	52	1090	43		80	319.3	430	200	1147	1038.11	0.91
M4	148.31 × 148.31 × 2.87	52	3101	26		80	319.3	430	200	931	844.70	0.91
M6	152.12 × 152.12 × 4.82	32	1105	41.5		80	316.6	430	200	1416	1331.35	0.94
M7	150.82 × 150.82 × 4.86	31	2199	21		80	316.6	430	200	1519	1412.68	0.93
M8	150.37 × 150.37 × 4.86	31	3100	25.5		80	316.6	430	200	1103	1094.06	0.99
Mean												0.96
Standard deviation (SD)												0.06
Coefficient of variation(COV)												0.06

($P_{u.num}$) to the experimental value ($P_{u.exp}$) is 0.96 with a standard deviation of 0.06 and the coefficient of variation of 0.06. Fig. 4 shows the predicted and experimental load-deflection curves for specimens L3 and L4. It can be seen from the figure that the numerical model predicts well the load-deflection responses of the specimens. It can be concluded that the numerical model yields good predications of the nonlinear inelastic behavior of normal and high strength CFST slender beam-columns.

6. Applications

The numerical model developed was used to investigate the effects of concrete compressive strength, loading eccentricity ratio (e/D), depth-to-thickness ratio (D/t) and column slenderness ratio (L/r) on the performance indices. The following parameters are kept constant in the present parametric study. The initial geometric imperfection at the mid-height of the beam-column was taken as $L/1500$. The yield and tensile strengths of the steel tubes were 690 and 790 MPa respectively. The Young's modulus of steel was 200 GPa.

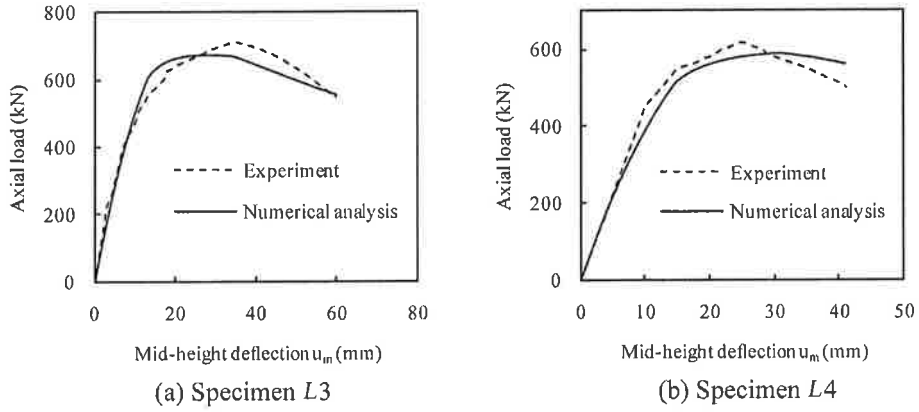


Fig. 4 Comparison of predicted and experimental axial load-deflection curves

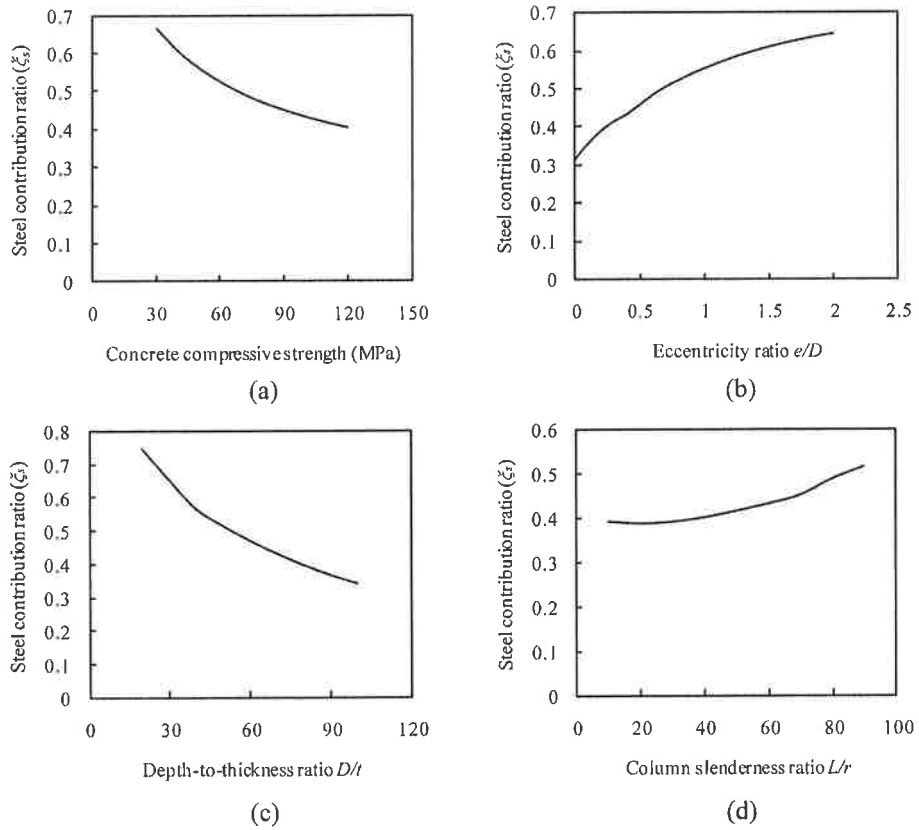


Fig. 5 Steel contribution ratio

6.1 Steel contribution ratio

A column cross-section of 600×700 mm was considered in the study of steel contribution ratio. The depth-to-thickness ratio of 70, the column slenderness ratio of 60 and the loading eccentricity

ratio of 0.4 were used to examine the effects of concrete compressive strengths. Fig. 5(a) shows that increasing the concrete compressive strength appreciably reduces the steel contribution ratio. The steel contribution ratio of a CFST slender beam-column with concrete compressive strength of 30 MPa is 0.67 and it is only 0.40 when 120 MPa concrete is used. Fig. 5(b) depicts the effects of the loading eccentricity ratio on the steel contribution ratio of the beam-column filled with 100 MPa concrete. It would appear from Fig. 5(b) that the steel contribution ratio considerably increases with increasing the end eccentricity ratio. For the end eccentricity ratios of zero and two, the steel contribution ratios are 0.31 and 0.65 respectively.

Fig. 5(c) illustrates the effects of depth-to-thickness ratio on the steel contribution ratio of CFST slender beam-columns filled with 100 MPa concrete. It can be seen from figure that the steel contribution ratio decreases with an increase in the depth-to-thickness ratio. This may be attributed to the fact that the steel area in column section and the local buckling strength of the steel tube decreases with an increase the depth-to-thickness ratio. The effects of column slenderness ratio on the steel contribution ratio of thin-walled CFST beam-columns are shown in Fig. 5(d). The steel contribution ratios are 0.39, 0.42 and 0.56 for the columns with slenderness ratios of 10, 50 and 90 respectively. This indicates that the use of slender columns increases their steel contribution ratio. Fig. 6 shows that local buckling remarkably reduces the stiffness and overall buckling strength of the CFST slender beam-column with the D/t ratio of 100, e/D of 0.4, L/r ratio of 40 and concrete compressive strength of 100 MPa. The overall buckling strength of the slender beam-column is overestimated by 6.73% if local buckling was not considered. This highlights the importance of considering local buckling effects in the inelastic stability analysis of thin-walled CFST slender beam-columns.

6.2 Concrete contribution ratio

The concrete contribution was evaluated on a CFST slender beam-column with the cross-section of 700×700 mm. To study the effects of concrete compressive strengths, loading eccentricity ratio of 0.4, the depth-to-thickness ratio of 50 and the column slenderness ratio of 35 were considered. It is observed from Fig. 7(a) that the concrete contribution ratio increases with an increase in the

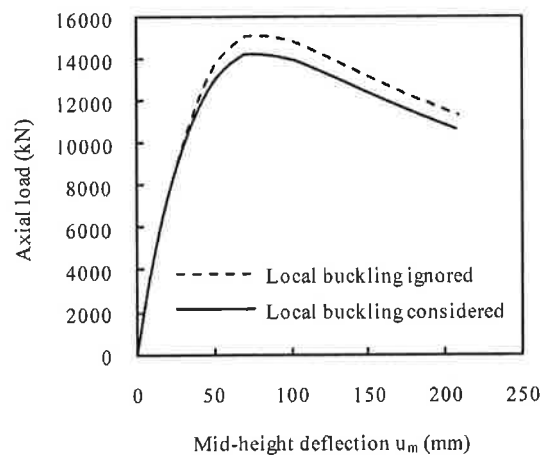


Fig. 6 Effects of local buckling on the axial load-deflection curve for thin-walled CFST slender beam-column

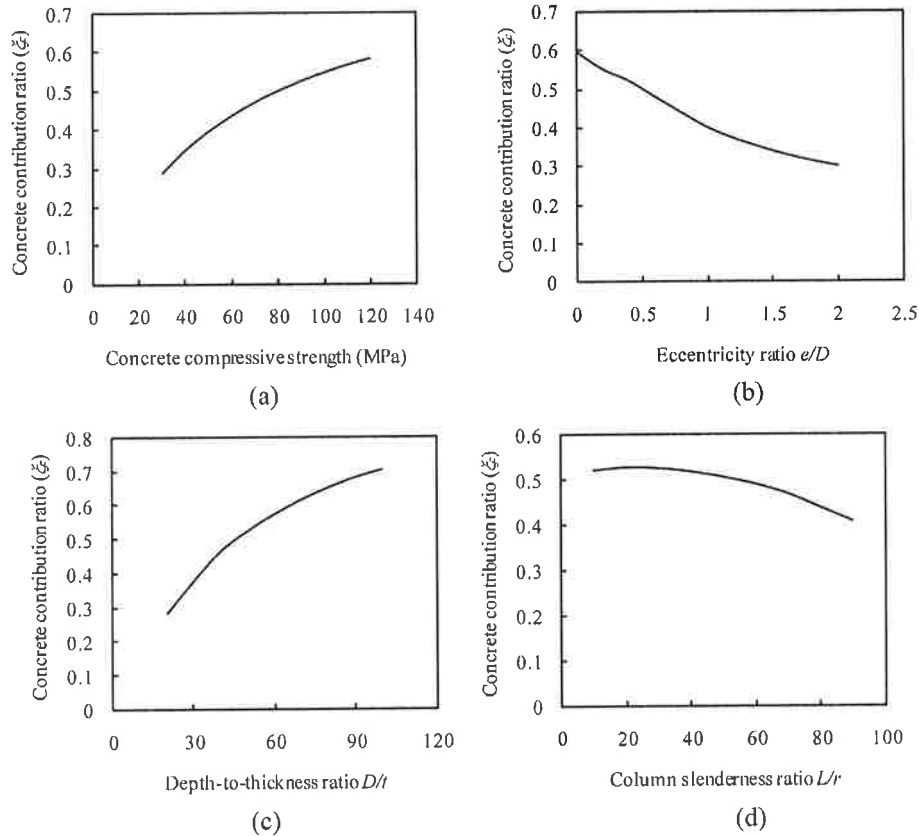


Fig. 7 Concrete contribution ratio

concrete compressive strength. Fig. 7(b) shows the effects of the loading eccentricity ratio on the concrete contribution ratio of the beam-column filled with 90 MPa concrete. It appears that increasing the loading eccentricity ratio significantly reduces the concrete contribution ratio of CFST slender beam-columns.

The effects of depth-to-thickness ratio and column slenderness ratio on the concrete contribution ratio of the beam-columns filled with 90 MPa concrete are shown in Fig. 7(c) and Fig. 7(d) respectively. It can be seen from Fig. 7(c) that increasing the depth-to-thickness ratio significantly increases the concrete contribution ratio. Fig. 7(d) shows that increasing the column slenderness ratio decreases the concrete contribution ratio.

6.3 Strength reduction factor

The cross-section of a CFST slender beam-column used in the analysis was 500×600 mm. The depth-to-thickness ratio of 60, loading eccentricity ratio of 0.4 and the slenderness ratio of 60 were used to study the effects of concrete compressive strengths. Fig. 8(a) indicates that increasing the concrete compressive strength significantly reduces the strength reduction factor. The effects of loading eccentricity ratio on the strength reduction factor of the beam-columns filled with 80 MPa concrete are presented in Fig. 8(b). It appears from Fig. 8(b) that the strength reduction factor

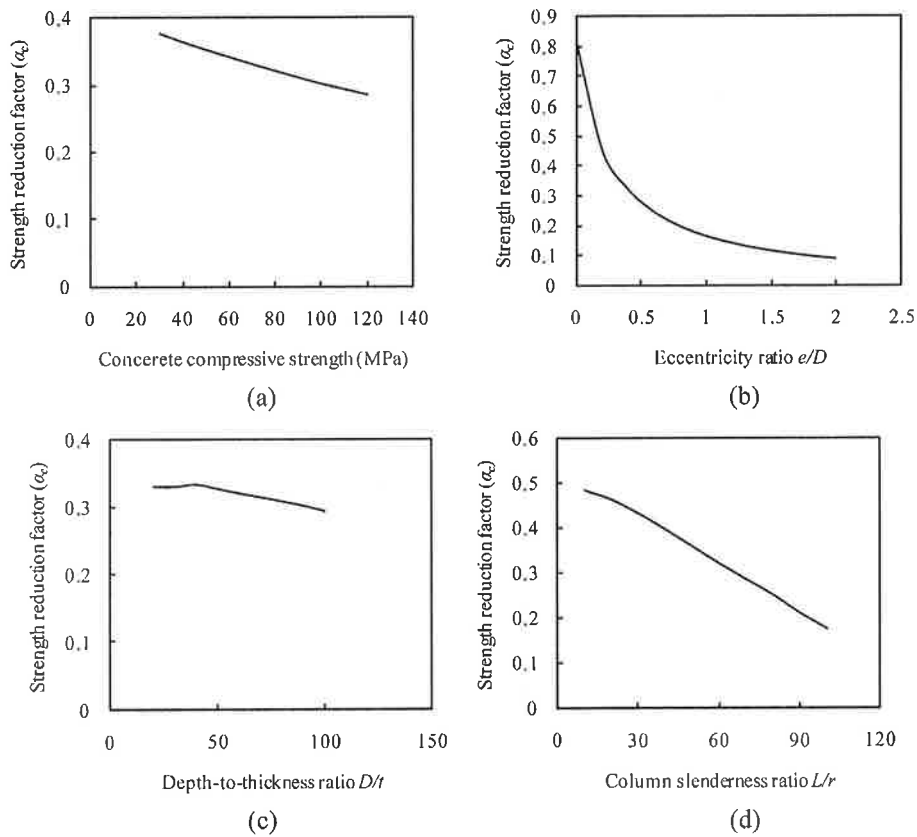


Fig. 8 Strength reduction factor

decreases with an increase in the e/D ratio. Fig. 8(c) shows the effects of depth-to-thickness ratio on the strength reduction factor of the columns with 80 MPa concrete. It can be seen from Fig. 8(c) that the strength reduction factor decreases with an increase in the D/t ratio for the same size composite section. As shown in Fig. 8(d), the strength reduction factor appears to decrease with an increase in its L/r ratio.

7. Conclusions

This paper has presented a multiscale numerical model for simulating the interaction local and global buckling behavior of high strength rectangular CFST slender beam-columns under axial load and bending. The effects of progressive local buckling of the steel tube walls under stress gradients are accounted for in the mesoscale model based on the accurate fiber element method. Computational algorithms have been developed to implement the macroscale model for predicting the load-deflection responses of high strength CFST slender beam-columns. The verification and applications of the multiscale model demonstrate that the multiscale numerical model developed is accurate and efficient for the inelastic stability analysis of high strength CFST slender beam-columns with large depth-to-thickness ratios.

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